E-Z EXCAVATING LLC.

2358 HWY# 23 MORA MN. 55051 Ph. 320-679-4031 Cell 320-241-7036

DESIGN

LOCATION: XXXXXX HWY 65 McGREGOR MN. PID# 30.0.027400 & 30.0.027500

OWNER: MILLE LACS BAND OF OJIBWE SYSTEM TYPE: TYPE III MOUND

DESIGN FLOW:2450 GPD

TREATMENT AREA: 10'X204' 2040 SQ.FT. **MOUND SIZE:** 40.8' X 232.4' **SLOPE: 2%**

SEPTIC TANKS: 3-2500 gal. COMBO/SPLIT FILTER: YES 3- POLYLOC

PUMP TANK: 5000 gal.

PUMP: GOULDS WE2012H

FLOW METER/ TIMER/ ALARM: SJE-RHOMBUS **TD1W114H8AC10EK21E**

muy # 1472 7/14/15

DESIGN NOTES

TYPE III MOUND SYSTEM: FLOW CALCULATIONS

9 RV SITES WITH FULL HOOKUPS @ 100 GPD. = 900 GPD. 24 CAMP SITES NO HOOKUPS WITH SHOWER HOUSE AND DUMP STATION @ 63 GPD. = 1512 GPD. TOTAL CALCULATED FLOW 2412 GPD. SYSTEM DESIGNED FOR 2450 GPD. WITH TIMED DOSING

SHOWER HOUSE IS SHOWERS ONLY NO TOILETS PORTABLE RESTROOMS WILL BE SET UP DURING EVENTS

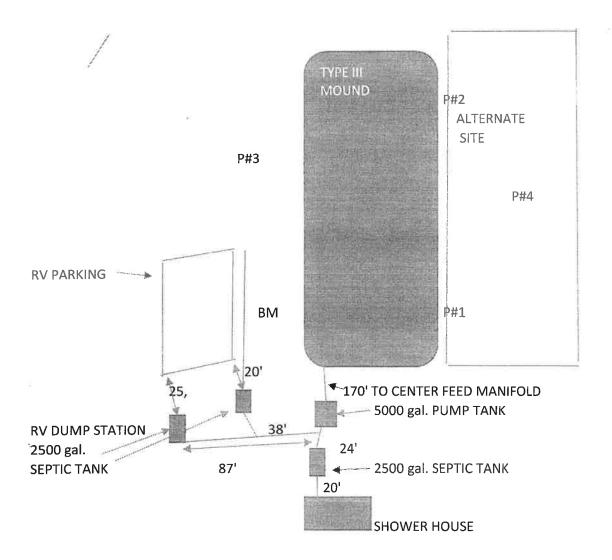
Site Elevation Sheet

LOCATION

BENCHMARK LOCATION:	STAKE BETWEEN MC	OUND AND RV PAI	RKING	ELEVATION 100.00
TANK #1 DUMP STATION	surface 96.10	inlet 94.25 C	OUTLET 94.00	
TANK #2 RV HOOKUPS	surface 97.00	inlet 94.25 O	UTLET 94.00	
TANK #3 SHOWER HOUSE	surface 97.30	inlet 93.25 O	UTLET 93.00	
PUMP TANK	surface 97.49	inlet 92.66 (OUTLET 92.50)
ROCK BED SURFACE				
N.E. 97.85				
N.W. 97.65				
S.E. 97.85				
S.W. 97.70				
BERM SURFACE				
N.E. 98.15				
N.W. 97.30				
S.E. 97.40				
S.W. 97.30				
S.W. 97.30 SAND TO ROCK BED INTE	RFACE ELEVATION:	100.85		
	RFACE ELEVATION:	100.85		
SAND TO ROCK BED INTE		100.85		
SAND TO ROCK BED INTE	REDOX 96.54	100.85		



NOT TO SCALE



ä.,

FIELD EVALUAT CIL

ADDRESS: LEGAL DESCRIPTION					
PINE 30.0.02740	0 and 500 SEC_	19 47 23	PNAME	OHWL	
FIRE#LAKE/			CL-58	OHWL	
DESCRIP DISTURBED AREAS COMPACTED AREAS FLOODING	TION OF SOIL TREA AREA #1 YES_XNO YES_NO YES_NO K	AREA ::		SM ELEV. <u>100</u> BM DESCRIPTION CC By Moun	1
RUN ON POTENTIAL	YES_NOX	YES HOY			
SLOPE % DIRECTION OF SLOPE LANDSCAPE POSITION VEGETATION TYPES	a construction and the second				
DEPTH TO STANDING	WATER OR MOTTL	ED SOIL: PICK	*1(8)" +2 (8"	1+2 (21) +41 (2)
	/CEIDER C				
BOTTOM ELEVATION-	FIRST TRENCH OR	BOTTOM OF PLC	<u> </u>	Frank H2	
SOIL SIZING FACTOR:	SITE # 1 .68	station and statio	. 68		
CONSTRUCTION RELAT	ED ISSUES:				
		2 8 C C C C C	/ .	/ -	
LIC# <u>1472</u>	SITE EVALUATO		turn the	wy	
SITE EVALUATOR NAME	KEVIN HERN	sia //	E EPHONE# 32	0 -241-7036	harring a
LUG REVIEW	1		ي. جو پي يلغو في		
Comments					
			-		
	SOIL BORIN	GLOGS OL REV	1.508		AGUNT.
		ATTACHED			

Form des 2/20/98

University of Minnesota Site Evaluation Forn 5/16/2005



Property Owner(s)	MILLE LACS B	AND OF OJIB	WE	Phone Numb	per 320-532-4	181
Address <u>3XXXX HWY</u>						
P.I.D. <u>30.0.027400</u> &		Section		· · _ · · · · · · · · · · · · · · · · ·	N Range	23
Date <u>7/14/2015</u>		Time 2PM	Weather conditi	ons OVERCAST		
Location Information	shoreland		dwelling		replacement	t system
(check all that apply)	protection area		\underline{X} other establishm	ent	new home c	construction
Homeowner Information						
No. of bedrooms (if applicable)	NONE	bedrooms (inclu	ides possible addition	ns)		
No. of residents in home	adults	children				
Estimated flow	2450	gpd				
Well casing depth	N/A	feet		Discharge location if che	ecked	
Water using devices (check)	Garbage disposal		Water softener			
	Dishwasher		 Sump pump			-
	Large bathtub		High eff. furnace		a 7	-
	Laundry/large tub	o on 2nd floor	Jucuzzi/hottub			
Water use concerns (check)	Toilet/faucet leak	s Max load lau	ndrv/day	Long term prescriptio	n medications	
	Home business		Antibact. soap	Frequent parties or ou		.c
				requent parties of of	it of town guest	.5
Soil Data						
Soil texture classification:	FINE SANDY LOA					
Unnatural soil (check)	X Yes	No				
Type of observation (check)	Probe	X Pit	Boring			
Parent material (check)	Till	X Outwash	Loess	Bedrock	Alluvium	
Vegetation type (check)	Wet	Dry	X Unknown			
Slope form (check)	X Summit	Shoulder	Back	Foot	Toe	
Drainage (check)	Good	X Fair	Poor	Ponding	Flooding	
Located in floodplain (check)	Yes	X No		· · · · · · · · · · · · · · · · · · ·		
				Soil Survey Data	Soil #1	Soil #2
Site Summary Data				Map unit sym & name	DULUTH	DULUTH
Standing water:		inches		Landscape position	SUMMIT	SUMMIT
Bedrock:		inches		Flooding		
Saturated soil:	8	inches		Slope	1 - 6%	1-6%
Maximum depth of system:	0	inches		Watertable depth		
Max elevation at system bottom:	100.85	feet		Bedrock depth		
Soil sizing factor (SSF):	0.68	gpd/ft ²		Possible system depth	0	0
Linear loading rate (LLR):	12	gpd/ft		Texture at depth	FSL	FSL
Was a perc test done ?	Yes		mpi	Permeability (P)		
	X No			Perc(MPI) = 60 / P		
				NRCS onsite suitability	V. LIMITEI	V. LIMITED

Soil Boring Data

Boring 1 Elevation:		Location			the state of the second
Soil Horizons Depth (inches)	Texture		Color	Structure	Consistence
	FIELD MIXED SOIL	10YR 3/3		NONE	FRIABLE
8"-12"	SANDY CLAY LOAM	10YR4/3	REDOX 7.5YR4/4	PLATY	FIRM
,					
					Ē.

Texture	Color	Structure	Consistence
FIELD MIXED SOIL	10YR3/3	NONE	FRIABLE
SANDY CLAY LOAM	10YR4/3 REDOX 7.5 YR4/4	PLATY	FIRM
	FIELD MIXED SOIL		FIELD MIXED SOIL 10YR3/3 NONE

	iversit Iinnesc		OSTP Soil (Observatior	Log		v 11.3.28	Date	7/14/2015 2PM	
Cl	ient/ Address	:				Land				
Legal Desc	ription/ GPS	PID 30.0.	027400 £ 500				Vegetation		IAY FIELD	
	nt materials . that apply)	🖸 Outw 🗹 Till	ash 🔲 Lacustrine	Loess edrock Organic		n #/Location: vey map units		3 Slope shape	Slope%	2.0
Depth (in)	Texture	Coarse Frag. %	Matrix Color(s)	Mottle Color(s)	Redox Kind(s)	Indicator(s)		I Structure Grade		
PLOWED SOIL 0-8	fine sandy loam	5	10YR3/3				Granular	Structureless	Friable	
8-12	sandy clay loam	5	10YR4/3	7.5YR4/4	Concentrations, depletions	S4	Platey	Weak	Firm	
								I		
			NPACTED SOILS							
	fy that I have o VIN HERWIG		this work in accordance	e with all applicable ordi	nances, rules and	aws.	1472		7/14/20	15
	(Designer)		1.1	(Signature)			(License #)	6	(Date)

Un of M	iversit [.] Iinneso	Y TA	OSTP Soil C)bservation	Log		v 11.3.28	Date	7/14/2015 2PM	
cı	lient/ Address:	×] Land	- Iscape position		SUMMIT	
Legal Desc	cription/ GPS	PID 30.0.	027400				Vegetation		IAY FIELD	
	nt materials l that apply)	🗌 Outw	ash 🔲 Lacustrine	Loess drock Organic		on #/Location:		4	Slope% 2.0	
					Soil sur	vey map units		Slope shape		
Depth (in)	Texture	Coarse Frag. %	Matrix Color(s)	Mottle Color(s)	Redox Kind(s)	Indicator(s)	Shape	Grade	eI Consiste	ence
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8-12	sandy clay loam	5	10YR4/3	7.5YR4/4	Concentrations, depletions	S4	Platey	Weak	Firm	
	-							-		
I hereby cert	OLD PLOWED ify that I have o EVIN HERWIG (Designer)	FIELD COA	APACTED SOILS this work in accordance	Kanus	nances, rules and	laws.	1472		7/14/20	
	(Designer)	*.e*		(Signature)	2		(License #)		(Date	?)



University of Minnesota Mound Design Worksheet Greater than 1% Slopes

lorouto						
Α.	FLOW					
~ .	Estimated		2450	gpd (see figure A-1)		
	or measured		2400	x 1.5 (safety factor) =	0	gpd
	or meddated					gpu
В.	SEPTIC TANK LIQUID VOLUMES					
	Septic tank capacity		7500	gallons (see figure C-1)		
	Number of tanks/compartments		6			
	Effluent Filter (yes/no)		YES	-		
				_1		
	C-1 Septic Tank Capacity in Gallons			1		
	Number of Minimum C	apacity with	Capacity with	1		
	Bedrooms Capacity (Garb. Disp.	Disp. and Lift			
	2 or less 750	1125	1500	1		
	3 or 4 1000	1500	2000			
	5 or 6 1500	2250	3000			
	7, 8 or 9 2000	3000	4000			
C.	SOILS (Site evaluation data)					
1.	Depth to restricting layer=		0.0	feet		
2.	Depth of percolation tests =		0.0	inches		
3.	Texture		FSL			
4.	Soil loading rate (see Figure D-33)		0.68	gpd/ ft ²		
4.	Percolation rate		0.00			
5.	% Land Slope		2.0	MPI %		
0.	to Land Clope		2.0	/0		
D.	ROCK LAYER DIMENSIONS					
1.	Multiply average design flow (A) by 0.83 to obtain requi	red area of rock	laver: Item A x 0.83=			
				0		
	2450gpd x 0.	83 ft²/gpd =		ft ²		
2.	Determine rock layer width = 0.83 ft ² /gpd x Linear Load	ling Rate (LLR)	(see LLR chart)			
	0.83 ft ² /gpd x	0 ()	12.00	= 10.0	ft	
	LLR Ch		1	-		
	Perk Ra <120 Mi		LLR	-		
	>=120 M		<=12 <=6			
_						
3.	Length of rock layer = area divided by width =					
	<u> 2040.0 </u> tt ²	1	10.0	feet =204.0	_ft	
E.	ROCK VOLUME					
1.	Multiply rock area by rock depth to get cubic feet of rock					
	2040.0	X	1.0	ft = 2040.0	ft ³	
	2010.0	X				
2.	Divide ft ³ by 27 ft ³ /yd ³ to get cubic yards					
2.		07 -	75.0			
	ft ³ /	27 =	75.6	_yd ³		
3.	Multiply cubic yards by 1.4 to get weight of rock in tons;					
э.		1 1 40-1-3	_	105.0		
	75.6yd ³ X	1.4 ton/yd ³		105.8tons		

Job #[

ABSORPTION WIDTH Absorption width equals		Absorption ratio:	2			
2.00	X X	10.0	ft =	20,0	ft	
				·	• .	
MOUND SLOPE WIDTI						
Downslope absorption v		•		10.0	<i>L</i> 1	
20.0	_feet -	10.0	feet =	10.0	ft	
Calculate mound size UPSLOPE						
a. Depth of clean sand a	at upslope edge of roc	k layer = 3 feet minus d	istance to restricting	layer(C1)		
3.0	ft	0.0	ft =	3.0	ft	
h Mariahi aitha i	valana adaa af vaale l	aver - darth of alarma	ad for a second in a (O)	0-)		
b. Mound height at the u at upslope edge plus de				2a)		
at upsiope edge plus de		3 ft + 1ft + 1 ft =	5.0	ft		
c. Upslope berm multipli		,				
	Selected berm mult	iplier:	2.83			
d I Inglang width — hann			(O0h)			
d. Upslope width = berm	2.83	upsiope mound neight(x	(G2D): 5.0	ft =	14.2 ft	
	2.00	- ^	0.0		<u> 14.2 </u> 11	
DOWNSLOPE						
e. Drop in elevation = ro	ck layer width (D2) tin	nes percent landslope(C	:5) / 100			
	10.0	_ft x	2.0	% / 100 =	ft	
f. Downslope mound hei	ight = depth of clean s	and for slope difference	e (G2e)			
at downslope rock edge			· · ·			
	0.2	_ft +	5.0	ft =	<u>5.2</u> ft	
g. Downslope berm mult	liplier based on percei Selected berm multi					
	Selected bern multi	plier:	3.19			
h. Downslope width = dc	wnslope multiplier(G;	a) times downslope mo	und height(G2f)			
·	3.19	x	5.2	=	16.6 ft	
		-	0			
i. Select greater of G1 ar	nd G2h as the downsl	ope width			<u> 16.6 ft</u>	
j. Total mound width is th	ne sum of unsione (G	2d) width plus rock laver	width (D2) plus dow	nelono width (C2i)		
ji rota mound mound a	14.2	ft +	10.0	ft +	16.6 ft =	40.8
		-	0		10.0	
k Total mound length is	the sum of upsiope w	iutin (Ozu) pius rock laye	er iengui (Do) pius up	osiope width (Gza)		
k. Total mound length is			204.0	ft +	14.2 ft =	232.4f
k. Total mound length is	14.2	- ^{ft} +	204.0			
k. Total mound length is			-			
	Final Dimensions (s	lope >1%)	4	0.8 ft x	232.4 ft	
k. Total mound length is	Final Dimensions (s	lope >1%)	4			
	Final Dimensions (s	lope >1%)	4	ces, rules & laws.	232.4 ft	Contection (Contection)

SAND VOLUME

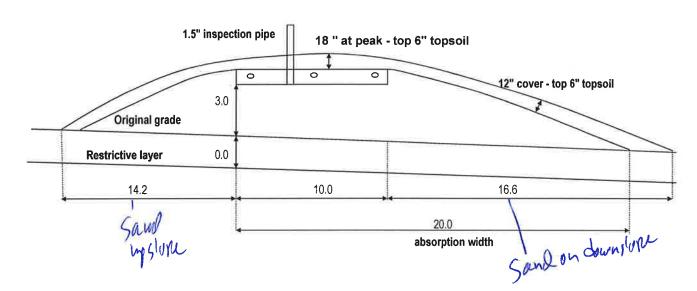
H.

1.	Upslope Volume + Volume	under rockbed + Do	wnslope Volume				
	a. Upslope Volume: (depth	of clean sand + 1) x	(upslope berm) x (mou	nd length) / 2 = ft^3			
	4.0	ft x	14.2	ft x	232.4	ft / 2 =	6600.2 ft ³
	b. Volume under rockbed:	(average depth of sa	nd under rock) x (rockb	ed width) x (mound le	$ength) = ft^3$		
	3.1	ft x	10.0	ft x	232.4	ft =	7204.4 ft ³
	c. Downslope Volume: (dej	pth of clean sand + 1) x (downslope berm) x	(mound length) / 2 =	ft ³		
	4.2	ft x	16.6	ft x	232.4	ft / 2 =	8101.5 ft ³
	Total cubic feet:	=	21906.0	ft ³		2	
2.	Divide ft ³ by 27 ft ³ /yd ³ to get	t cubic yards					
		21906.0	/ 27 =	811.3	yds ³		
3.	Multiply cubic yards by 1.4	to get weight of sand					
	_	811.3	yds ^{3 x} 1.4	1135.9	tons		
4	Add 10% for Constructability	у					
	_	1135.9 t	ons x 1.1 =	1249.5	tons		

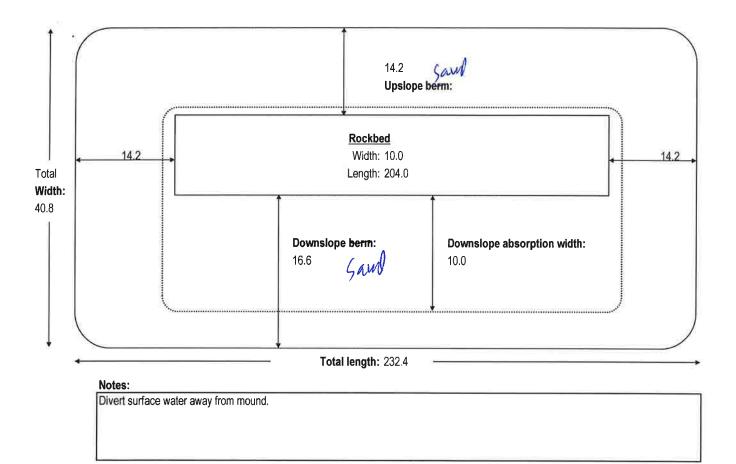
No. of				
Bdrms	Class I	Class II	Class III	Class IV
2	300	225	180	60% of
3	450	300	218	the
4	600	375	256	values
5	750	450	294	in the
6	900	525	332	Class I,
7	1050	600	370	ll or ll
8	1200	675	408	columns

Perc Rate mpi	Soil Texture	Loading Rate gpd/sq ft	Absorption
	Coarse sand	gpu/sq it	Ratio
<5	Loamy sand	1.20	1.00
	Med., Fine sand		
6 -15	Sandy loam	0.79	1.50
16-30	Loam	0.60	2.00
31-45	Silt Loam, Silt	0.50	2,40
46 - 60	Clay loam, Silty or Sandy Clay Loam	0.45	2.67
61-120	Silty or Sandy Clay or Clay	0.24	5
120*		0.24	5

Land			Upslope		Downslope						
%		m	ultipliers for variou	IS	multipliers for various						
Slope			slope ratios		slope ratios						
	3:1	4:1	5:1	6:1	3:1	4:1	5:1	6:1	7:1		
0	3.00	4.00	5.00	6.00	3.00	4.00	5.00	6.00	7.00		
1	2.91	3.85	4.76	5.66	3.09	4.17	5.26	6.38	7.53		
2	2.83	3.70	4.54	5.36	3.19	4.35	5.56	6.82	8.14		
3	2.75	3.57	4.35	5.08	3.30	4.54	5.88	7.32	8.86		
4	2.68	3.45	4.17	4.84	3.41	4.76	6.25	7.89	9.72		
5	2.61	3.33	4.00	4.62	3.53	5.00	6.67	8.57	10.77		
6 7	2.54	3.23	3.85	4.41	3.66	5.26	7.14	9.38	12.07		
	2.48	3.12	3.70	4.23	3.80	5.56	7.69	10.34	13.73		
8 9	2.42	3.03	3.57	4.05	3.95	5.88	8.33	11.54	15.91		
9	2.36	2.94	3.45	3.90	4.11	6.25	9.09	13.04	18.92		
10	2.31	2.86	3.33	3.75	4.29	6.67	10.00	15.00	23.33		
11	2.26	2.78	3.23	3.61	4.48	7.14	11.11	17.65	30.43		
12	2.21	2.70	3.12	3.49	4.69	7.69	12.50	21.43	43.75		
13	2.17	2.62			4.95	8.29					
14	2.13	2.55			5.24	8.92					
15	2.09	2.48			5.55	9.57					
16	2.06	2.41			5.88	10.24					
17	2.03	2.35			6.24	10.94					
18 19	2.00	2.29			6.63	11.67					
	1.97	2.23			7.04	12.42					
20	1.95	2.18			7.47	13.19					
21	1.93	2.13			7.93	13.99					
22 23	1.91	2.08			8.42	14.82					
	1.89	2.03			8.93	15.67					
24	1.87	1.98			9.46	16.54					
25	1.85	1.93			10.02	17.44					



Mound Detail: Land slope > 1%



University of Minnesota Pump Selection Procedure - 10/25/04 All boxed rectangles must be entered, the rest will be calculated.

 $\left(i \right)$

	 A. Gravity Distribution 1. Minimum required discharge is 10 gpm 2. Maximum suggested discharge is 45 gpm For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device. 	LIMI C	-00	÷	
	B. Pressure Distribution - see pressure design worksheet			point o	
	Selected Pump Capacity: 120 gpm	total pipe length		1	
2. A.	Determine Total Dynamic Head (TDH) Inlet Elevation difference between pump and point of discharge. Inlet 14 feet	2/	\. elevati differen		
В.	Special head requirement? (See Figure - Special Head Requirements)				
	5 feet	Special He			
C.	Friction loss in supply pipe	Gravity Dis Pressure D		Oft 1 5ft	
	1. Select pipe diameter 3 in				
	2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1)				
	Read friction loss in feet per 100 feet from Figure E-9	E-9 Frictio	n Loss ir	Plastic	Pipe
	Friction loss≃ 1.4 ft/ 100 ft of pipe		per 100		
			n	ominal	
	3. Determine total pipe length from pump discharge to soil system discharge point.	Flow Rate	pi	oe diame	ter
	Estimate by adding 25 percent to pipe length for friction loss in fittings.	(gpm)	1.5"	2.0"	3"
	Pipe length times 1.25 = equivalent pipe length	20	2.47	0.73	0.1
	175 ft x 1.25 = 218.75 feet	25	3.73	1.11	0.16
		30	5.23	1.55	0.23
	Calculate total friction loss by multiplying friction loss (C2)	35	6.96	2.06	0.3
	by the equivalent pipe length (C3) and divide by 100.	40	8.91	2.64	0.39
	Friction Loss = <u>1.4</u> ft/100ft X <u>218.75</u> ft / 100 = <u>3.1</u> feet	45	11.07	3.28	0.48
		50	13.46	3.99	0.58
D.	Total head requirement is the sum of elevation difference (A), special	55		4.76	0.7
	head requirements (B), and total friction loss (C4).	60	5 - 3 - A	5.6	0.82
	<u> 14 ft + 5 ft + 3.1 ft</u>	65		6.48	0.95
	Total Head: 22.1 feet	70		7.44	1.09
3.	Pump Selection				
	1. A pump must be selected to deliver at least120gpm (1A or B)with at least22.1feet of total head (2D).				
hei	reby certify that I have completed this work in accordance with all applicable ordinances,	rules and laws	i.		
_	wand the (signature) 1472 (license #)	77/15/ 2015			

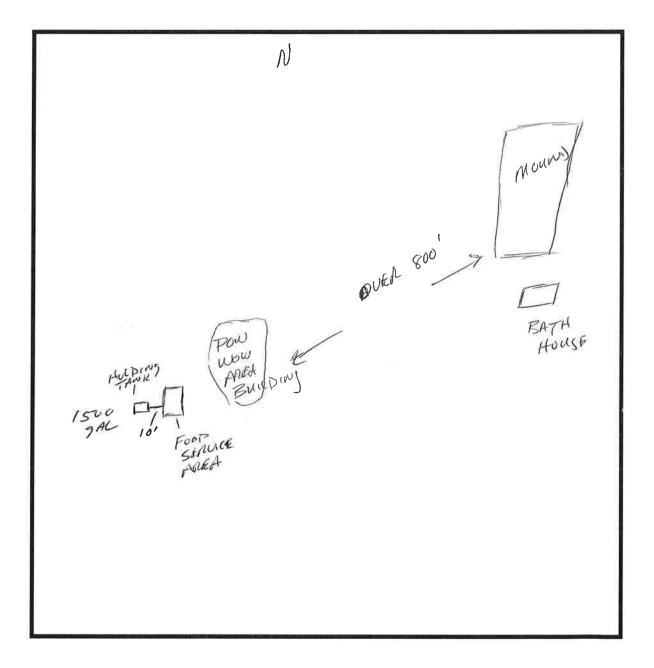
University of Minnesota Dosing Chamber Sizing with a Timer All boxed rectangles must be entered, the rest will be calculated.

1.	Determine area A. Rectangle area = L x W B. Circle area = $3.14 \times \text{radius}^2$			Widt	h	
	3.14 x 2 ft = 0.0 ft ² C. Get area from manufacture ft ²	Leng	th	$\left(\right)$		
2.	Calculate gallons per inch There are 7.5 gallons per cubic foot of volume, therefore multiply the area (1A, B or C) times the conversion factor and divide by 12 inches per foot to calculate gallon per incl Surface area x 7.5 / 12 = 0.0 ft ² x 7.5 / 12in/ft = 70.1 gallon per MANUFACTURER	h.		Legal Tank 00 gallons		
3.	Calculate recommended capacity = average design flow (see chart A-1) x 2 2450 gpd x 2 =gal		1009	% the daily ternating F	flow	
4.	Calculate total tank volume	ī —				
	A. Depth from bottom of inlet pipe to tank bottom = 72 in	1	ated Sewage F	lows in GPD		
	B. Total tank volume = depth from bottom of inlet pipe to tank bottom(4A) x gal/in(2) = <u>72</u> in x <u>70.1</u> gal/in = <u>5044.3</u> gallons	Number o Bedrooms 2		Class II 225	Class III	Clas
5.	Calculate gallons to cover pump (with 2-3 inches of water covering pump) (Pump and block height + 2 inches) x gallon per inch(2) (14]+ 2 in) x70.1gal/in =1121.0_gallons	3 4 5	450 600 750	300 375 450	218 256 294	the valu
6.	Calculate total usable tank volume total tank volume in gallons (4) - gallons to cover pump(5) 5044.3 gal - 1121.0 gal = 3923.4 gal	5 7 8	900 1050 1200	525 600 675	332 370 408	Clas II or colur
	A. Select pump size for 4-5 doses per day. Gallon per dose = gpd (see Figure A-1) / d 2450 gpd / 4 doses/day = 612.5 gallons B. Calculate drainback 1. Determine total pipe length 2. Determine liquid volume of pipe, 0.38 gal/ft (see figure E-20)	loses per da	y = E-20 Volume Pipe Diameter inches 1			
	2. Determine induit volume of pipe, $_$ 0.38 gaint (see ingure 2-20) 3. Drainback quantity = 175 ft (7B1) x 0.38 gal/ft(7B2) 66.5 C. Total pump out volume = dose volume(7A) + drainback (7B3) <u>612.5</u> gallons + 66.5 gallons = 679.0 gallons	_gallons	1.25 1.5	0.078		
8.	3. Drainback quantity = 175 ft (7B1) x 0.38 gal/ft(7B2) 66.5 C. Total pump out volume = dose volume(7A) + drainback (7B3)	_gallons _gpm	1.25	0.078		
8. 9.	3. Drainback quantity = <u>175</u> ft (7B1) x <u>0.38</u> gal/ft(7B2) <u>66.5</u> C. Total pump out volume = dose volume(7A) + drainback (7B3) <u>612.5</u> gallons + <u>66.5</u> gallons = <u>679.0</u> gallons Pump Rate From design <u>120</u> gpm or calculated: <u>change in depth</u> (in) x gallon per inch(2) / time interval in min = gpm	_gpm	1.25 1.5 2 2.5 3 4	0.078 0.11 0.17 0.25 0.38 0.66		
9.	3. Drainback quantity = <u>175</u> ft (7B1) x <u>0.38</u> gal/ft(7B2) <u>66.5</u> C. Total pump out volume = dose volume(7A) + drainback (7B3) <u>612.5</u> gallons + <u>66.5</u> gallons = <u>679.0</u> gallons Pump Rate From design <u>120</u> gpm or calculated: change in depth (in) x gallon per inch(2) / time interval in min = gpm in x <u>70.1</u> gal/in / min = <u>0.0</u> Calculate the timer ON setting Dose gallons(7C) / gpm (8)	_gpm	1.25 1.5 2 2.5 3 4	0.078 0.11 0.17 0.25 0.38 0.66		- con
9. 10.	3. Drainback quantity = <u>175</u> ft (7B1) x <u>0.38</u> gal/ft(7B2) <u>66.5</u> C. Total pump out volume = dose volume(7A) + drainback (7B3) <u>612.5</u> gallons + <u>66.5</u> gallons = <u>679.0</u> gallons Pump Rate From design <u>120</u> gpm or calculated: change in depth (in) x gallon per inch(2) / time interval in min = gpm in x <u>70.1</u> gal/in / <u>min = 0.0</u> Calculate the timer ON setting Dose gallons(7C) / gpm (8) <u>679.0</u> gal / <u>120.0</u> gpm = <u>5.7</u> minutes ON Calculate the timer OFF setting minutes per day / doses per day - minutes on	_gpm	1.25 1.5 2 2.5 3 4	0.078 0.11 0.17 0.25 0.38 0.66		alas con puripo corrito

<u>(</u>

AITKIN COUNTY BUILDING PERMIT SITE PLAN

Please indicate the location of: Wells, well setback to system components, buildings, septic system components, reserved septic system area, property lines, waterways, and buried lines. Include size, length, and appropriate distances from fixed reference points. Provide a North directional arrow!



	boxed rectangle											
1.	Select num	ber of perfor	rated laterals	8:	3	ONSITE Sewage Treatm Progra	E S					
2.	Select perfo	pration spaci	ing = [3]ft							
3.		the rock lay er length		ram), subtr	r that 1 foot to ract 2 feet from _ft		nan fatter to de la contra contra Contra contra c	eotextile fabric 9 of 1 9 of 1 9 zing 37 (6° - 17)? 9pacing 3.5'- 3'		-		
4.		ength (3) by		spacing (2)) and round do	own to nearest 3ft =	whole nun 67	ıber.	11			
5.	Select perfo	oration size	Ĩ	2]inch							
6.	* Check figu < 10% disch	ıre E-4 to as	sure the nui on.	mber of pe		erforation spac lateral guarant ateral						
	E-4 Maximu	N					auna Munak	or of 2/46 in	ob no foro	41		
	per lateral t							per of 3/16 in tee <10% dis				
	Perforation Spacing		Pipe Diame	tor		Perforation Spacing	n	Dine Diem	- 4			
	ft	1 inch	1.25 inch	1.5 inch	2.0 inch	feet	1 inch	Pipe Diam 1.25 inch		2.0 incl	h	
	2.5	8	14	18	28	2.5	12	19	25	39		
	3.0 3.3	8	13 12	17 16	26 25	3	11	18	24 23	37		
	4.0	7	11	15	23	4	10	16	21	33		
	5.0	6	10	14	22	5	9	15	20	31		
I	1. Rock bed 10 2. Square fo	ded value is l area = rock ft x pot per perfo	6-10 sqft/pe width (ft) x 204 foration=Rock	erf. Does n rock lengtl t = k Bed Area	n. ot apply to at-g h (ft) <u>2040</u> ft ² i/number of pe	rfs(6)			1 Ger	M. J	700 . V (19)	split we
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0	ded value is l area = rock ft x pot per perfo ft ² / equired flow ns(6A) by flo	6-10 sqft/pe k width (ft) x 204 f pration=Rock 204 p rate by mult	perforation arf. Does n rock length t = k Bed Area berfs = tiplying the rations (se	n. ot apply to at-g h (ft) <u>2040</u> ft ² //number of pe <u>10.0</u> ft ² , total number e figure E-6)	grades. rfs(6) / perf	apm	M	I Get	N. J.	JW. V	split way
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is area = rock ft x ft x pot per perform ft² / equired flow ns(6A) by flow	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult w per perfo perfs x	perforation erf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59	n. ot apply to at-o h (ft) <u>2040</u> ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs =	grades. rfs(6)	_gpm	M	y get	N. J.	100 . V (100)	split from a
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is area = rock ft x ft x pot per perform ft² / equired flow ns(6A) by flow	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult w per perfo perfs x t tion Discha	perforation erf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59	n. ot apply to at-c h (ft) <u>2040</u> ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = M	grades. rfs(6) / perf	_gpm	M	y Gel	N. J	7.10 ³	split way
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is a area = rock ft x bot per perfo ft ² / equired flow ns(6A) by flo 204 E-6 Perfora	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult w per perfo perfs x tion Discha Perfor	perforation erf. Does n rock lengtl t = k Bed Area berfs = tiplying the rations (se 0.59 rge in GP ations dian (inches)	n. ot apply to at-o h (ft) 2040 ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter	grades. rfs(6) / perf	_gpm	M	y Gel	N.	700 . V	split un
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is a area = rock ft x pot per perfo ft ² / 	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult by per perfo perfs x tion Discha Perfore 3/16	perforation erf. Does n rock lengtl t = & Bed Area berfs = liplying the rations (se 0.59 rge in GP ations dian (inches) 7/32	n. ot apply to at-g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter 1/4	grades. rfs(6) / perf	_gpm	M	y Gel	N. J.	JW	split way
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is area = rock ft x pot per perform	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult w per perfo perfs x tion Discha Perfor	perforation erf. Does n rock lengtl t = k Bed Area berfs = tiplying the rations (se 0.59 rge in GP ations dian (inches)	n. ot apply to at-o h (ft) 2040 ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter	grades. rfs(6) / perf	_gpm	M	y Gel	N. J	700 . V ~ (193)	split way
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine record of perforation	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo 204 p E-6 Perform Head (feet) 1^{9} 2^{9} 5	6-10 sqft/pe width (ft) x 204 f paration=Rock 204 p rate by mult ov per perfo perfs x tion Discha Perfor: 3/16 0.42 0.59 0.94	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GPI ations dian (inches) 7/32 0.56 0.80 1.26	n. ot apply to at $\frac{1}{2040}$ ft ² $\frac{2040}{100}$ ft ² $\frac{10.0}{100}$ ft ² total number e figure E-6) gpm / perfs = M neter $\frac{1/4}{0.74}$	grades. rfs(6) / perf	_gpm	M	y Gel	N.	V . WY	split un
[- 8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is a area = rock ft x bot per perform ft ² /	6-10 sqft/pe width (ft) x 204 f paration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GPI ations dian (inches) 7/32 0.56 0.80 1.26 ly homes.	n. ot apply to at $\frac{1}{100}$ h (ft) <u>2040</u> ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04	grades. rfs(6) / perf	_gpm	M	N Gel	N.	N. V. (U) V	split wa
8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo _204 _ p E-6 Perform Head (feet) 1^{a} 2^{o} 5 a. Use 1.0 foot b. Use 2.0 feet	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x t tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GPI ations dian (inches) 7/32 0.56 0.80 1.26 ly homes.	n. ot apply to at $\frac{1}{100}$ h (ft) <u>2040</u> ft ² i/number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04	grades. rfs(6) / perf	_gpm	4	I Get	M.	JW	split way
8.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation	ded value is a area = rock ft x bot per perfor ft ² / equired flow ns(6A) by flo 204 Fe-6 Perfora Head (feet) 1^{a} 2^{a} 5 a. Use 1.0 foot b. Use 2.0 feet	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor: 3/16 0.42 0.59 0.94 for anything els e Size	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 ly homes. e	n. ot apply to at- (ft) 2040 ft ² //number of pe 10.0 ft ² , total number e figure E-6) gpm / perfs = M neter 1/4 0.74 1.04 1.65	grades. rfs(6) / perf	_gpm	4	Y Gel	N.	7 (19) V	split un
9. A.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in 1	ded value is a area = rock ft x	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor: 3/16 0.42 0.59 0.94 for anything els e Size erals are con to solect mir	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 y homes. e nected to l	h. ot apply to at- g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral	grades, hfs(6) / perf <u>120.4</u>	•	4	contractory A Statestary	M.	7 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	split un
9. 4 A. 1	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; ent	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo 204 Te-6 Perform Head (feet) 1^a 5 a. Use 1.0 foot b. Use 2.0 feet linimum Pipe End. If late Figure E-1, if ter figure E-1	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor: 3/16 0.42 0.59 0.94 for anything els e Size trals are con to solect mir 4 or E-5 with	perforation arf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 y homes. e nected to l nimum require perforation	n. ot apply to at-g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 <u>1.04</u> <u>1.65</u> header pipe uired lateral on spacing anc	grades, hfs(6) / perf <u>120.4</u>	•	1	contractory A Statestary	M - M	Ju . V	Split un
9. A. C.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; ent	ded value is a area = rock ft x pot per perform ft ² /	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor: 3/16 0.42 0.59 0.94 for anything els e Size trals are con to solect mir 4 or E-5 with	perforation arf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 y homes. e nected to l nimum require perforation elect minim	h. ot apply to at- g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral	grades, hfs(6) / perf <u>120.4</u>	•	1	contractory A Statestary	M M	2~10 ³	split un
9. 1 A. 1	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in diameter; end number of perforated	ded value is a area = rock ft x bot per perform ft ² / - equired flow ns(6A) by flo 204 p E-6 Perform Head (feet) 1^8 2° 5 a. Use 1.0 foot b. Use 2.0 feet Figure E-1, flate Figure E-1, fla	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els e Size prats are conn to solect mir 4 or E-5 with er lateral. S	perforation erf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rrge in GPI ations dian (inches) 7/32 0.56 0.80 1.26 binum requi- perforation elect minin	h. ot apply to at-g h (ft) 2040 ft ² /number of pe 10.0 ft ² total number e figure E-6) gpm / perfs = M neter 1/4 0.74 1.04 1.65 header pipe wired lateral on spacing and num diameter inches	grades, hfs(6) / perf <u>120.4</u>	I: Manifold Loca	sted al End of Syste	contractory A Statestary	M -	2 100	split un
9. / A. I G.	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; ent number of perforated Center Mani manifold pipe	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo _204 pr E-6 Perform Head (feet) 1^{a} 2° 5 a. Use 1.0 foot b. Use 2.0 feet Figure E-1, i ter figure E-1, i ter figure E-2, i ter figure E-3, i ter figure E-4, i	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x t tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els e Size rals are con to solect mir 4 or E-5 with er lateral. So perfor lateral perfor single-famil	perforation arf. Does n rock length t = k Bed Area berfs = tiplying the rations (se 0.59 rge in GPI ations dian (inches) 7/32 0.56 0.80 1.26 by homes. e nected to I nimum requires perforation elect minim al system is gure E-2, p	n. ot apply to at-g h (ft) <u>2040</u> ft ² //number of pe <u>10.0</u> ft ² , total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral on spacing and num diameter inches s attached to perforated late	grades, Infs(6) / perf <u>120.4</u> Higure L- Higure L-	I: Manifold Loo	1	contractory A Statestary	M - 1 M	Ju ivi	split un
9. / A. I B. (r f	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; end number of perforated Center Mani manifold pipe and number of	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo _204 pr E-6 Perform Head (feet) 1^{a} 2° 5 a. Use 1.0 foot b. Use 2.0 feet Figure E-1, 1 linimum Pipe Figure E-1, 1 ler figure E-2, 1 erforations p d laterals = fold. If performation	6-10 sqft/pe width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els e Size erals are con to sclect mir 4 or E-5 witt er lateral. Se orated lateral enter, like Figures	perforation arf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 y homes. e nected to I himum requi- perforation elect minin al system is gure E-2, p al (5) will b	n. ot apply to at-g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral on spacing and num diameter inches s attached to perforated late e approximate	grades, Infs(6) / perf <u>120.4</u> Higure L- Higure L-	I: Manifold Loo	aled al End of Syste	contractory A Statestary	M - 1 M	2 100	split un
9. / A. I B. (r f B. (Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; ent number of perforated Center Manifold pipe and number of perforated Center Manifold pipe and number of th	ded value is a area = rock ft x bot per perform ft ² / equired flow ns(6A) by flo _204 _ p E-6 Perform Head (feet) 1^{a} 2° 5 a. Use 1.0 foot b. Use 2.0 feet Figure E-1, 1 der figure E-1, 1 for the figure E-1 erforations p d laterals = fold. If performation at in step A.	6-10 sqft/pe (width (ft) x 204 f pration=Rock 204 p rate by mult ow per perfo perfs x tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els e Size prats are con to solect mir 4 or E-5 witt er lateral. So corated latera enter, like Fig ns per lateral.	perforation arf. Does n rock length t = k Bed Area berfs = hiplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 binum requint perforation elect minin al system is gure E-2, p al (5) will bise values,	n. ot apply to at-g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² , total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral on spacing and hum diameter inches s attached to perforated late e approximate select	grades, rfs(6) / perf <u>120.4</u> Higure L- Higure L- Higure L- Higure L-	I: Manifold Loo	aled al End of Syste	contractory A Statestary	M - 4	2 100	split un
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9. 8. B. B. C T	Recommend 1. Rock bed 10 2. Square for 2040.0 Determine re of perforation Determine M Manifold on as shown in I diameter; end number of perforated Center Mani manifold pipe and number of one half of th minimum diameter	ded value is a area = rock ft x pot per perform ft ² / - equired flow ns(6A) by flo 204 p E-6 Perform Head (feet) 1^{47} 2° 5 a. Use 1.0 foot b. Use 2.0 feet Figure E-1, iter figure E-1, er forations p d laterals = fold. If performe ence are the co of perforation at in step A, meter for pe	6-10 sqft/pe (width (ft) x 204 f paration=Rock 204 p rate by mult ow per perfo- berfs x tion Discha Perfor 3/16 0.42 0.59 0.94 for single-famil for anything els e Size erals are con to select mir 4 or E-5 with er lateral. Se corated latera berfor the figure series are con to select mir 4 or E-5 with er lateral. Se corated latera berforated latera	perforation arf. Does n rock length t = k Bed Area berfs = liplying the rations (se 0.59 rrge in GP ations dian (inches) 7/32 0.56 0.80 1.26 ly homes. e nected to I nimum requ perforation elect minim al system is gure E-2, p al (5) will b se values, pral =	n. ot apply to at-g h (ft) <u>2040</u> ft ² /number of pe <u>10.0</u> ft ² total number e figure E-6) gpm / perfs = <u>M</u> neter <u>1/4</u> 0.74 1.04 1.65 header pipe uired lateral on spacing and num diameter inches s attached to perforated late e approximate <u>select</u> <u>2</u> inc	grades, hrfs(6) / perf <u>120.4</u> Hgure L- Hgure L- Hgure L- Hgure L-	I: Manifold Loca Figure 6:2 In the Cel	aled al End of System	and Dimetaria		2	Split un
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AITKIN COUNTY ENVIRONMENTAL SERVICES

APPLICATION for an OPERATING PERMIT FOR WASTEWATER TREATMENT AND DISPERSAL

PERMITTEE	PARCEL NUMBER	R_30.0.027	400 £ 500
ADDRESS XXXX HWYH65	Mc CAEGON	Mn.	-
LEGAL DESCRIPTION			-
TELEPHONE #	GIS LOCATION	J.	-):
A. DESCRIPTION OF WASTEWATER TREA (Attach ISTS site evaluation and design construction, operation, monitoring, ser management; anticipated system life, hy 	estimated cost of size, component re	system	

B. MONITORING PLAN AND REPORTING FREQUENCY:

PARAMETER	COMPLIANCE LIMIT	SAMPLE LOCATION	SAMPLE FREQUENCY	SAMPLE TYPE	REPORTING FREQUENCY
FLOW	2450	CYCLUE CONSTUER	AFTER EVENT		
5-DAY BOD	P		6).		
TOTAL NITROGEN					
TOTAL PHOSPHORUS					
TSS					
FATS,OILS AND GREASE					
FECAL COLIFORM					
SEPARATION DISTANCE	3'	MOUND	AN.		

OWNER

will perform the monitoring of this septic system.

C. MAINTENANCE PLANS

	PARAMETER	LOCATION	FREQUENCY
	solids remain 1	Septie tamles	annul
¥) i	perf trate & Almin	pomptant	
1	Eschunt Filter	Aug Septe Tamic	
	Flow	chile countr-	4
	CLEAN' FILTER	EVERY 30-90 DAYS OF S EVERY 36 MONTHS	(AS NEEDED (RECURD) (RECURD)
	RECERD METE	ER READINGS EVERY 3	BO DAYS
	CHECK MOUN	D FOR SEEPAGE EVEN	Y 30 DAYS
	D. MITIGATION PLAN	N: OCCURS NOTIFY AND	KIN COUNTY AND
	E-7 EXCAULT	NG AS SOON AS POSSIB	LE.
	DISCONNECT TI	HE MOUND PUMP AND U LS UNITIL THE PROBLE	SE THE TANKS AS
	CALL & SEPTIC	PUMPING COMPANY AND	SET UP A PUMPING
	CONTRACT.		

I hereby certify with my signature as the designer, that all data for the operating permit application is true and correct to the best of my knowledge. I agree to indemnify and hold Aitkin County harmless from loses, damages, costs and charges that may be incurred by the County because of the information submitted with this application.

Signature

1412 License Number

<u>7-14-15</u> Date

1520 E Alaple AUE Munder 320-679-403/ Address Telephone #

KEVIN HERWIG

Name (please print)

c:operatpermit.doc

MAINTENANCE SERVICE. MONITORING AND INSPECTION CONTRACT FOR INDIVIDUAL SEWAGE TREATMENT SYSTEM

It is hereby agreed this ____ day of _____ by and between (Inspector) and (client)

(Client) Name & Address_ MILLE LACS BAND OF OTIBWE

Street Address XXXV Hwy H 65-City, State, Zip Mc Gregor MN.

That in consideration of the payments provided herein, the Inspector shall provide services to perform Preventative Maintenance, Monitoring and Inspection of the Individual Sewage Treatment System (ISTS) located at the property described in the Aitkin County Operating Permit.

Each inspection includes an examination of the ISTS followed by a written report to the client. This inspection report shall contain recommendations for operation and maintenance for failure-preventative measures, if any are deemed appropriate by the inspector and a list of recommended corrective measures or replacement parts. The Inspector is authorized to submit a copy of the report to the Aitkin County Environmental Services Department.

This contract does not assume any responsibilities or obligations, which are normally the responsibilities of the Client, as related to parts or labor and does not extend to cover any costs that may be associated with any recommendations made under this contract.

The Inspector can only contract or subcontract for parts or labor after authorization. Billings for service calls shall be made on a case by case basis. This contract only covers maintenance, monitoring and inspection services per current Aitkin County Operating Permit and does not cover alarm calls of any kind.

The Inspector shall be provided access to the site and the system in order to perform the following services:

SEPTIC TANK AND LIFT STATIONS INSPECTION

(check the boxes needed to fill the requirements of the Operating Permit)

Check septic tank and compartments for solids buildup and general appearance. If necessary, have tanks pumped (cost of pumping is the responsibility of the client).

Check effluent filter for buildup and clean, if applicable,

Check pumping system, including control panel and floats.

 $\underline{\checkmark}$ Record and date the readings of the elapsed time meter and cycle counter(s), if applicable.

Check dosing settings (in the control panel, if applicable).

___ Other: _____

**If the septic tank or lift stations need pumping to be in compliance with the operating permit the cost of the pumping is the responsibility of the Client.

TREATMENT DEVICE

Inspect pretreatment unit (aerobic tank, sand filter, etc.) per manufacturer's recommendations, if applicable.

Inspect and clean any parts per manufacturer's recommendations.

____ Inspect and clean laterals, if applicable.

_____ Inspect the appearance of the wastewater inside the unit for color, turbidity and examination of odors.

____ Sample effluent per Operating Permit monitoring requirements.

(Cost of sampling and analysis is the responsibility of the Client)

_ Other: _____

DISPERSAL FIELD

Inspect for visible signs of failure (surface discharge, soggy ground, wet spots, settling, etc.)

____ If liquid level monitors are installed, levels will be observed and recorded.

Flush filters and clean cartridges, if applicable.

____ Check field control unit solenoid operations or manual control, if applicable.

____ Other: _____

In no event shall the Inspector be responsible for special or consequential damages, including but not limited to, loss of time, injury to personal property or any other consequential damages or incidental or economic loss due to equipment failure or for any other reason. This contract does not assume any responsibilities or obligations, which are normally, the responsibility of the Client or as, related to parts or labor and does not extend to cover any costs that may be associated with any recommendations made under this contract.

This contract shall be effective: Beginning _____, ____,

and Ending _____, ____,

Cost for Maintenance Service, Monitoring and Inspection Contract is:

\$_____/yr. For _____ years totaling \$______

The Inspector agrees to provide inspection, monitoring and routine maintenance service only under this contract. The Client remedies for breach of this contract shall be limited to refund of any of the amounts paid in advance for service. This contract may be renewed 30 days from the ending date.

Payment for	all services shall be paid	
Client:	Inspector:	C
Sign:	Mille Law Hand will do own d Sign:	Nain Enana,
Print:	Print:	
Date:	Date:	