# FIELD EVALUATION SHEET

PRELIMINARY EVALUATION DATE 5/12/2016 , FIELD EVALUATION DATE 5/12/2016	
MORERIT OWNER: Donna M. Kellar (Wiese)  PHONE M/A	
AUDRESS: 38252 Deer St. CITY STATE 7IP Aitkin MN 56431	
LEGAL DESCRIPTION: PT OF SW NE (TRACT B & 1/6 OF 1/4 TH THE THE DEVICED TO SW	DI
24-0-013901 SEC 8 1 46 R 26 1M/P NAMENTARIA	ן ע
FIRE#LAKE/RIVER_Nord_Lake LAKE CLASS RD OHWIn/a	
CHILD OLHOO RD OHIVI III A	
DESCRIPTION OF SOIL TREATMENT AREAS	
ADELA III	
DISTUDDED ADEAS	
COMPACTED AREAS VES NO VES	ION
FLOODING YES NO X YES NO X Center of small cement	
A 123 NO A pad www corner of exis	tin
SLODE W	
DIDECTION OF SUCRE	
LANDOOAGE	
VECETATION TYPES	
VEGETATION TYPESlawn	
DEPTH TO STANDING WATER OR MOTTLER COLL PORMAN	
DEPTH TO STANDING WATER OR MOTTLED SOIL: BORING# 1 4', 1A , 23.75,2A	
BOTTOM ELEVATION EIRST TRENCH OF BOTTOM OF BOOK BETTOM	
BOTTOM ELEVATIONFIRST TRENCH OR BOTTOM OF ROCK BED: #1 100.3 FT., #2	FT.
SOIL SIZING EACTOR, OTT #4	
SOIL SIZING FACTOR: SITE # 1 2.00 , SITE #2	
CONCEDUCTION DEL ATTENDO	
CONSTRUCTION RELATED ISSUES: Replacement system for an existing cabin. The ol	d
tank is to be insp. & reused and a 520 gal. pump tank, added.	
(1860 combo to be installed if old tank bad.)	
IC#L1392 SITE EVALUATOR SIGNATURE:	
SITE EVALUATOR NAME: Charles Marshula TELEPHONE# 218-927-3619	
TELETIONET 210 J27-J01J	
UG REVIEW DATE	
DATEDATE	
Comments:	
SOIL BORING LOGS ON REVERSE SIDE	
ONSITE INSPECTION	
NO ONSITE INSPECTION	
INO CHOILE INSPECTION	
Form des 2/20/98 5-16-16 5-16-16	
Form des 2/20/98	

## SOILS CHARTS FOR BOTH PROPOSED AND ALTERNATE SITES

1 (PROPOSED) SOILS DATA

# DEPTH | TEXTURE | MUNSELL |

OC1 111	ILEXTORE	MONSE	
(INCHES)		COLOR	
0-6"	Topsoil		
6"-24"	Fine Sandy	Loam	10YR4/
24"-24"	Loam/Sand		10YR5/
	9		1
No mott	ling observ	ed	
	27/2		
*			

#### 2 (PROPOSED) SOILS DATA

	DEPTH	TEXT	URE N	UNSELI	Karr	
	(INCHES)»		, (C	OFOR-		_
	0-7"	Topso	oil			
	7"-28"	Fine	Sandy	Loam	10 YR	4/4
	28"-45"	Loam	Sand	10YF	25/4	
	( <u>4</u> )		:4			
	No mott	ling (	observ	ed	1/7	
1						

1 (ALTERNATE) SOILS DATA

#### 2 (ALTERNATE) SOILS DATA

NCHES)	TEXTORE .	COLOR	1		(INC	ES)	N/E	ooi Mu	OR SELEN
There which	is 300'+ would be	between suitable	the pro	posed s	ite ate	and Deer site.	St.	All	of
	ce .								
20	*							a.	



Job#	
OOD III	1 1

# University of Minnesota Mound Design Worksheet Greater than 1% Slopes

			M						
A.		FLOW							
		Estimated	*		450	gpd (see figui	•		
		or measured				x 1.5 (safet	y factor) =	0	gpd
В.		SEPTIC TANK LIQUID V	OLUMES						
		Septic tank capacity			1250	gallons (see f	icure C-1)		
		Number of tanks/compart	ments		2	- ganons (occ )	iguro e i,		
		Effluent Filter (yes/no)			no	1			
		,			<del></del>				
		C-1 Septic Tank Capaci	ty in Gallons						
		Number of	Minimum	Capacity with	Capacity with	1			
		Bedrooms	Capacity	Garb. Disp	Disp. and Lift	1			
		2 or less	750	1125	1500				
		3 or 4	1000	1500	2000				
		5 or 6	1500	2250	3000				
		7, 8 or 9	2000	3000	4000				
C.		SOILS (Site evaluation de	ata)						
	1.	Depth to restricting layer=	•		2.0	]feet			
	2.	Depth of percolation tests			2.0	inches			
	3.	Texture			Fine Sandy Loam	4		100	
	4.	Soil loading rate (see Figu	ure D-33)		0.60	gpd/ft <sup>2</sup>			
		Percolation rate	,		0.00	MPI			
	5.	% Land Slope			2.0	%			
_									
D.		ROCK LAYER DIMENSION							
	1.	Multiply average design fl	ow (A) by 0.83 to obt	ain required area of roc	k layer: Item A x 0.83=				
		_	450	$gpd \times 0.83 ft^2/gpd =$		380	ft <sup>2</sup>		
	2.	Determine rock layer widt	h = 0.83 ft <sup>2</sup> /apd x Lin	ear Loading Rate (LLR)	(see LLR chart)				
			0.83 ft²/gpd x	<b>3</b> ( ,	12.00	=	10.0 ft		
					12.00	_	10.0		
			,	LLR Chart		]			
				Perk Rate	LLR				
				<120 MPI	<=12				
				>=120 MPI	<=6				
	3.	Length of rock layer = area							
		2	380.0	ft <sup>2</sup> /	10.0	feet =	38.0 ft		
E.		ROCK VOLUME			,	` = '	. <del></del>	*);	
	1.	Multiply rock area by rock	depth to get cubic fe	et of rock					
	550	marapiy room as as a y room	380.0	X	1.0	4 -	380.0 ft <sup>3</sup>		
		-	300.0	^	1.0	ft =	ft <sup>3</sup>		
	2.	Divide ft <sup>3</sup> by 27 ft <sup>3</sup> /yd <sup>3</sup> to g	et cubic vards						
		amadir by ar itryd to g	•	t <sup>3</sup> / 27 =	44.4	3س			
		-	300.0	1 21 =	14.1	yd³			
;	3.	Multiply cubic yards by 1.4	to get weight of rock	in tons;					

\_\_\_\_\_14.1 yd³ X

19.7

1.4 ton/yd<sup>3</sup> =

ABSORPTION WIDTH Absorption width equals	absorption ratio time	Absorption ratio:		2					
2.00	X	10.0	ft	=		20.0	ft		
	- "	- 10.0	-		-	40.0	- "		
MOUND SLOPE WIDT	H & LENGTH (Great	er than 1%)							
Downslope absorption v	width = absorption wid	dth minus rock layer wi	dth						
20.0	feet -	10.0	feet =			10.0	ft		
***************************************	_				,	,		2	
Calculate mound size					(3)				
UPSLOPE									
a. Depth of clean sand	at upslope edge of ro	ck layer = 3 feet minus	distance to	restrictin	g layer(C	1)			
3.0	ft -	2.0	ft =		, , ,	10	ft		
					-				
b. Mound height at the i	upslope edge of rock	laver = depth of clean	sand for se	paration ((	32a)				
at upslope edge plus d				paradon (	<i></i>		93		
		1 ft + 1ft + 1 ft =	. 1001,	3.0	_ft	25			
			*)	0.0					
c. Upslope berm multipl	ier based on land slo	pe (see figure D-34)							
о, орокоро воли пискр	Selected berm mul	• • •		3 70					
	Colobica Somminar	приог		370					
d. Upslope width = bern	n multiplier/G2c\ time	e unelono mound hoid	**(C2b)·						
u. opsiope widin - bein	3.70		II(GZD).	2.0		<b>a</b> ==	4.4	4 6	
	3.70	_ x	-	3.0		ft ≝	11	<u>.1</u> ft	
DOWNSLOPE	7								
	and devices which (DO) 4		(05) / 100		4)			750	
e. Drop in elevation = ro			(C5) / 100						
	10.0	_ ft x	<del>( , , , , , , , , , , , , , , , , , , ,</del>	2.0	— %	/ 100 =	0,	2ft	
f. Downslope mound he									
at downslope rock edge	-		of rock lay						
	0.2	_ <sup>ft</sup> +		3.0	ft =		3.	2ft	
	e. e. i								
g. Downslope berm mul		· -	ure D-34)						
	Selected berm mul	tiplier.	1	4.35					
h. Downslope width = d		62g) times downslope r	nound heig	ht(G2f)					
	4.35	_ ×		3.2		=	14	<u>.0</u> ft	
£									
i. Select greater of G1 a	ind G2h as the downs	slope width					14	<u>.0</u> ft	
: Total manual width in i	dha arma ai malama //	20-A							
j. Total mound width is t			er wath (L			wath (G			05
	11.1	ft +	***************************************	10.0	ft +		14	<u>.0</u> ft =	35
k. Total mound length is	the sum of upslope	width (G2d) plus rock l	ayer length	(D3) plus	upslope v	width (G2	d)		
	11.1	ft +		38.0	ft +		11	.1 ft =	60
		_ " '	-	30.0	"		-	· <del></del> " -	
	Final Dimensions	(slope >1%)			35.1	ft x		60.2 ft	
I hereby certify that all v	vork has been compli	eted in accordance wit	n all applica	ble ordina	inces, rul	es & laws	3		
	11/16.	4			411			6/12/	// (date
Marles.	XI Brains	(signature)	[ 1740	)	11100	ህርው #/\			
Charles a	A (mgms	(signature)	L139	2	(lice	nse #)		1/15/	(0010

Page 2 of 5

#### H. SAND VOLUME

1. Upslope Volume + Volume under rockbed + Downslope Volume

a. Upslope Volume: (depth of clean sand + 1) x (upslope berm) x (mound length)  $/ 2 = ft^3$ 

2.0	ft	X	11.1	ft	X	60.2	ft /2 =	668.2	ft <sup>3</sup>
b. Volume under rockbed:	(average	depth o	f sand under rock) x (rockbed	width) x	(mound	length) = ft <sup>3</sup>			
1.1	ft	X	10.0	ft	X	60.2	ft =	662.2	ft <sup>3</sup>
c. Downslope Volume: (de	epth of cle	an sand	+ 1) x (downslope berm) x (m	nound len	gth) / 2	= ft <sup>3</sup>			
2.2	ft	X	14.0	ft	x	60.2	ft / 2 =	927.1	ft <sup>3</sup>
Total cubic feet:	:	=	2257.5	fi	3				

2. Divide ft³ by 27 ft³/yd³ to get cubic yards

	2257.5	/ 27 =	83.6	yds
Multiply cubic yards by	1.4 to get weight of san	d in tons		
	83.6	yds <sup>3 x</sup> 1.4	117.1	tons

4 Add 10% for Constructability

3.

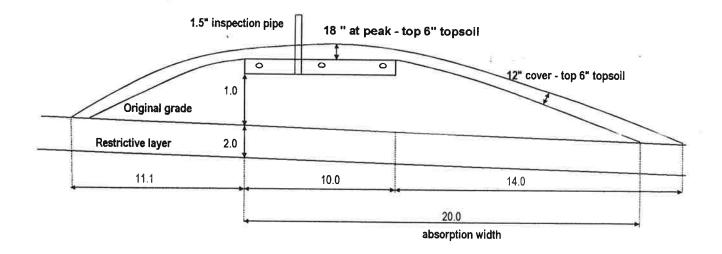
117.1	tons x 1.1 =	128.8	tons

No. of				
Bdrms	Class I	Class II	Class III	Class IV
2	300	225	180	60% of
3	450	300	218	the
4	600	375	256	values
5	750	450	294	in the
6	900	525	332	Class I,
7	1050	600	370	ll or il
8	1200	675	408	columns

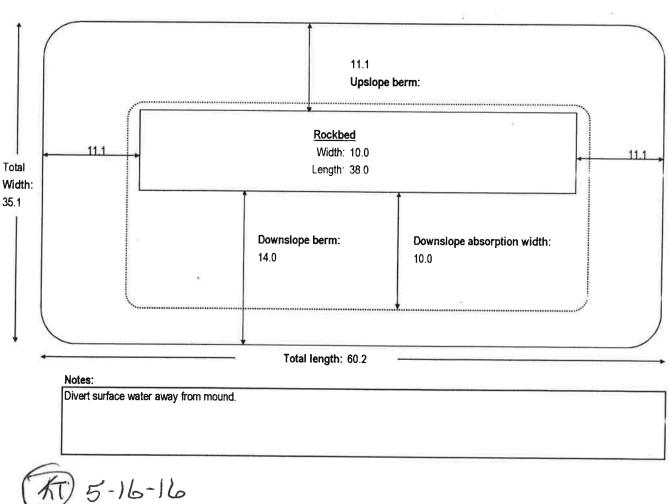
Perc Rate	Soil Texture	Loading Rate	Absorption
mpi		gpd/sq ft	Ratio
	Coarse sand	DE PRESENTATION DE LA CONTRACTION DE L	
<5	Loamy sand	1.20	1.00
	Med., Fine sand		
6 -15	Sandy loam	0.79	1.50
16-30	Loam	0.60	2.00
31-45	Silt Loam, Silt	0.50	2.40
46 - 60	Clay loam, Silty	0.45	2.67
	or Sandy Clay Loam		
61-120	Silty or Sandy	1. Surger 1. Surger 1.	
	Clay or Clay	0.24	1 5
120*			

S-16-16

Land			Upslope		Downslope						
%		mu	tipliers for variou	ıs		mult	ipliers for vario	ous			
Slope		slope ratios			slope ratios						
	3:1	41	5:1	6,1	3:1	4:1	5:1	61	7:1		
0	3.00	4.00	5.00	6.00	3 00	4.00	5 00	6.00	7 00		
	2.91	3.85	4.76	5.66	3.09	4.17	5.26	6.38	7,53		
2	2.83	3.70	4.54	5.36	3.19	4.35	5.56	6.82	8.14		
3	2.75	3.57	4.35	5.08	3.30	4.54	5.88	7.32	8.86		
4	2.68	3.45	4.17	4.84	3,41	4.76	6.25	7.89	9.72		
5	2.61	3.33	4.00	4.62	3.53	5.00	6.67	8.57	10.77		
6	2.54	3.23	3.85	4.41	3.66	5.26	7.14	9.38	12.07		
7	2.48	3.12	3.70	4.23	3,80	5.56	7.69	10.34	13.73		
8	2.42	3.03	3 57	4.05	3 95	5.88	8 33	11.54	15 91		
9	2.36	2.94	3.45	3.90	4.11	6.25	9.09	13.04	18.92		
10	2.31	2.86	3.33	3.75	4.29	6.67	10.00	15.00	23.33		
11	2.26	2.78	3.23	3.61	4.48	7.14	11:11	17.65	30.43		
12	2.21	2.70	3.12	3.49	4.69	7.69	12.50	21.43	43.75		
13	2.17	2.62			4.95	8.29					
14 15	2.13	2.55			5.24	8.92					
	2.09	2.48			5.55	9.57			10		
16	2.06	2.41			5 88	10.24					
17	2.03	2.35			6.24	10.94					
18	2.00	2.29			6,63	11.67					
19	1.97	2.23			7.04	12.42					
20	1.95	2.18			7.47	13.19					
21	1.93	2.13	175		7.93	13.99					
22	1,91	2.08			8,42	14.82					
23	1.89	2.03			8,93	15.67					
24	1.87	1.98			9.46	16.54					
25	1.85	1.93			10.02	17.44					



Mound Detail: Land slope > 1%



		5	
	in the second se		
1 · · · · · · · · · · · · · · · · · · ·	v.		

١.		SHWAGE				
	Select number of perforated laterals: 3	PROGRAM		-7F-		
2.	Select perforation spacing = 2.5 ft					
١.	Since perforations should not be placed closer that 1 foot to	Ç	Geo	textile fabric	minimi	
	the edge of the rock layer (see diagram), subtract 2 feet from	Quart	or unch perforati	Se o( t	ock ock	-
	37.5 - 2 ft = 35.5 ft	1	Perí Sea Perí Sea	ing 3/16" - 1/4" Sing 1.5" - 5'		
			,,,			
٠.	Determine the number of spaces between perforations.  Divide the length (3) by perforation spacing (2) and round down	to postoct who	olo pumbor			
		ft =	14	•		
	Solvet restaurtion also			-		
•	Select perforation size 1/4 inch					
	Number of perforations is equal to one plus the number of perform					
	* Check figure E-4 to assure the number of perforations per late < 10% discharge variation.	erai guarantee:	s			
	14 spaces + 1 = 15 perforations/late	eral				
	E-4 Maximum Number of 1/4 inch perforations	E-5 Maximu	m Numbe	r of 3/16 inc	ch norforat	ione
	per lateral to guarantee <10% discharge variation	per lateral to				
	Perforation Spacing Plpe Diameter	Perforation Spacing		Pipe Diame	ntor	
	ft 1 inch 1.25 inch 1.5 inch 2.0 inch	feet	1 inch	1.25 inch	1.5 inch	2.0 inch
	2.5 8 14 18 28 3.0 8 13 17 26	2.5	12	19	25	39
	3.0 8 13 17 26 3.3 7 12 16 25	3.3	11 10	18 17	24 23	37 36
	4.0 7 11 15 23	4	10	16	21	33
	5.0 6 10 14 22	5	9	15	20	31
	B. Calculate the square footage per perforation.  Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10  ft x	(6)				
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)	6) perf				
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf	gpm			
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad  1. Rock bed area = rock width (ft) x rock length (ft)  10  ft x	6) perf	gpm			
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10  ft x	6) perf	gpm			
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad  1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf	gpm			
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)   10	6) perf	<b>g</b> pm	¥ =	, le	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)   10	6) perf	gpm	ŭ :	, le	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)   10	6) perf	gpm	morn parties	e le	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf	<b>Jpm</b>		one from comp	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)   10	6) perf	Jpm	and delivery of the second		
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf 33.3 _ g		move to the second of Systems	THE POST OF	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf 33.3 _ g		nor party	THE POST OF	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf 33.3 _ g		non package and all End of Syste	THE POST OF	re.
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g	Manifold Locate	lanifold Located	THE POST OF	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g	Manifold Locate		THE POST OF	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g	Manifold Locate	lanifold Located	THE POST OF	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g	Manifold Locate	lanifold Located	THE STATE OF THE S	
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g  Regure E-1: N	Figure 5-2-M In the Center	familioid Located t of the System	To the state of th	Joseph Control of the
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g  Regure E-1: N	Figure 5-2-M In the Center	familioid Located t of the System	To the state of th	Provide the second
	Recommended value is 6-10 sqft/perf. Does not apply to at-grad 1. Rock bed area = rock width (ft) x rock length (ft)  10	6) perf  33.3 g  Regure E-1: N	Figure 5-2-M in the Center	familioid Located t of the System	7 ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	Provide the second

### University of Minnesota Pump Selection Procedure - 10/25/04

All boxed rectangles must be entered, the rest will be calculated.

#### Determine pump capacity:

#### A. Gravity Distribution

- 1. Minimum required discharge is 10 gpm
- 2. Maximum suggested discharge is 45 gpm

For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device.



B. Pressure Distribution - see pressure design worksheet

Selected Pump Capacity:

33.3 gpm

Determine Total Dynamic Head (TDH)

Elevation difference between pump and point of discharge.



- C. Friction loss in supply pipe
  - 1. Select pipe diameter
  - 2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1)

Read friction loss in feet per 100 feet from Figure E-9

Friction loss= 2.06 ft/ 100 ft of pipe

3. Determine total pipe length from pump discharge to soil system discharge point. Estimate by adding 25 percent to pipe length for friction loss in fittings.

Pipe length times 1.25 = equivalent pipe length

93.8 feet
93.8

4. Calculate total friction loss by multiplying friction loss (C2)

by the equivalent pipe length (C3) and divide by 100.

Friction Loss = 2.06 ft/100ft X 93.8 ft / 100 : feet

D. Total head requirement is the sum of elevation difference (A), special head requirements (B), and total friction loss (C4).

ft + 5 ft + 1.9 ft

Total Head: 14.9 feet

total pipe

length

Inlet III

pipe

Special Head Requirements 0ft

difference

soll treatment system

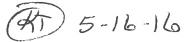
Gravity Distribution Pressure Distribution 5ft

	E-9 Friction Loss in Plastic Pipe per 100 ft						
		ominal					
Flow Rate	pip	e diame	ter				
(gpm)	1.5"	2.0"	3"				
20	2.47	0.73	0.11				
25	3.73	1.11	0.16				
30	5.23	1.55	0.23				
35	6.96	2.06	0.3				
40	8.91	2.64	0.39				
45	11.07	3.28	0.48				
50	13,46	3.99	0.58				
55		4.76	0.7				
60		5.6	0.82				
65	The second	6.48	0.95				
70	<b>沙库斯斯</b>	7.44	1.09				

#### 3. Pump Selection

1. A pump must be selected to deliver at least gpm (1A or B) with at least feet of total head (2D).

hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws. (license #) 5/13/2016 L1392



			DOSING CI	HAMBER SIZI	NG - 10/25/0	4	-			
	•	must be entered,	the reșt will be ca	alculated			1		Wid	th
1,	A Rectangle ar	ea = L x W	<b>4</b>		٦.	•	ft² ←			
	B. Circle area =		ft x	l	]ft =	0	_π	Length		
	C. Get area from	3.14 x m manufacture		'ft =	0.0	_ft²			Radi	ius
2_	times the conver	allons per cubic fo rsion factor and di	vide by 12 inches	refore multiply the a	e gallon per inch					
	Surface area x 7	7.5 / 12 =	0	_ft² x 75 / 12ir	n/ft =	16.6 (From Manuf	gallon per inch acturer)		Legal Tank 500 gallons	
3(	Calculate total tan					143 ·			100% the daily	flow
			to tank bottom bottom of inlet o	= ipe to tank bottom(3	31.5 (A) x gal/in/2)	in		0	r Alternating P	umps
	=	31.5	in x	16.6	gal/in =	522.3	gallons			
4				f water covering pur	np)					
	(Pump and blod		s) x gallon per ind + 2 in) x	ch 16.6	_gal/in =	232.1	gallons			
5. (	Calculate total pur						4 -		8	
		size for 4-5 doses gpd /	s per day. Gallon 5	per dose = gpd (se doses/day =	e Figure A-1) / dos 90	es per day = _gallons				
	lack _			-		7	Edward L			
		Sewage Flows In	GPD			4	E-20 Volume of L			
	Number of Bedrooms	Class I	Class II	Class III	Class IV		Pipe Diameter inches	Liquid per foo gallons	1	
	2	300	225	180	60% of	1	1	0.045		
	3	450 600	300 375	218 256	the	1	1,25 1,5	0.078		
	5	750	450	294	values in the		2	0.110 0.170		
	6	900	525	332	Class I,	1	2.5	0.250		
	7	1050	600	370	II or II		3	0.380		
	8	1200	675	408	columns	J	4	0.660		
	<ol> <li>Determine</li> <li>Drainback</li> </ol>	total pipe length liquid volume of p quantity = out volume = dose	pipe, 75.0 volume(5A) + dra galloņs +	75.0 0.17 ft (5B1) x ainback (5B3) 12.8	ft gal/ft (see figure 0.17 gallons =	e E-20) _gal/fl(5B2) = 102.8	12.8 _gal	_ <sup>gal</sup> inlet_ pipe	ogpac	
6. 0		oaration distance olume(5C) / gal/in gal /	(using total pump ch(2) 16.6	out volume) gal/in =	6,2	_inch	*		COURT COURT	
7.		e for alarm (typica th) x gallon/inch(2		2	in x	16.6	_gal/in =	33.16ga	liihmmmm	
8.		allons = gallons o gal +	ver pump(4) + ga 102.8	llons pumpout(5C) · _gal +	+ gallons alarm(7)	_gal =	368.0	_gal		
9		= total gallons(8) gallons /	/ gallon/in(2) 16 58	_gal/in =	22 2	_in				
	ommended						1			
	culate reserve cap y flow x 0.75 =	pacity (75% of the	daily flow) 450	x 0.75 =	337.5	gallons				
		-7								
l he	eby certify that I	hare completed th	nis work in accord	lance with all applica	able ordinances, ru	iles and laws				
0	harked	Vinni	(signature)	L1392	-	_(license #)	5/13/2016			
		· · · · · · · · · · · · · · · · · · ·								

KT 5-16-16

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CLIENT: DATE: MAP DRAWN TO SCALE WITH A NORTH ARROW NORD >100' DEEP WELL 112' TO TANK 116' TO ROCKRED EXIST 3 BDR OLD SEEPAGE RED CABIN Per Installer a new NEW PUMP TANK EL 99.1 BM EL 100 58#1 EXIST. GAR SB#-2 > 300' TO DEER ST. CHECK OFF LIST--HAVE ALL OF THE FOLLOWING BEEN DRAWN ON THE MAP?? SHOW EXISTING OR PROPOSED

☐ WATER WELLS WITHIN 100 FT OF TREATMENT AREAS
PRESSURE WATER LINES WITHIN 10 FT OF TREATMENT AREAS
☐ STRUCTURES ☐ LOT IMPROVEMENTS
ALL SOIL TREATMENT AREAS ALL ISTS COMPONENTS
☐ HORIZONTAL AND VERTICALREFERENCE
POINT OF SOIL BORINGS DIRECTION OF SLOPE
□ LOT EASEMENTS     □ ALL LOT DIMENSIONS
DISTURBED/ COMPACTED AREAS
SITE PROTECTION—LATHE AND RIBBON EVERY 15 FT
ACCESS ROUTE FOR TANK MAINTENANCE
REQUIRED SETBACKS
STRUCTURES PROPERTY LINES
NOHWL
COMMENTS: (KT) 5-16-16,
DESIGNER SIGNATURE MANUA (MUMA)
LICENSE# L 1302
LIOLINOLH L 139V

#### **INDICATE ELEVATIONS**

DATE 5/13/16

BENCHMARK	1 Di
ELEVATION OF SEWER LINE @ HOUSE	96
ELEVATION @ TANK INLET (PUMD)	94:
<b>ELEVATION @ BOTTOM OF ROCK LAYER</b>	R/00.
ELEVATION @ BOTTOM OF BORING OR	
RESTRICTIVE LAYER 9	5,6
ELEVATION OF PUMP 92	2.3
ELEVATION OF DISTRIBUTION DEVICE	101
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6 c s			

# **Subsurface Sewage Treatment System Management Plan**

Property Owner: <u>Donna M. Kellar (Weise)</u>	Phone:	Date: <u>5/13/16</u>
Mailing Address: 2709 S.Garfield Ave.	City: Sioux Falls, SD	Zip:_ 57015
Site Address: 38252 Deer St.	City: Aitkin, MN.	Zip:56431
	-	
This management plan will identify the operation and main performance of your septic system. Some of these activities must be performed by a licensed septic service provider.	ntenance activities necessary to enses must be performed by you, the h	sure long-term omeowner. Other tasks
	months. My System ne	eds to be checked
	months. every 36	months.
(State requirements are based on MN Rules Chapter 7080.2450, Subp. 2		
Homeowner Management Tasks	,	
Leaks - Check (look, listen) for leaks in toil	ets and dripping faucets. Repair lea	ks promptly.
Surfacing sewage – Regularly check for we	t or spongy soil around your soil tre	eatment area.
Effluent filter – Inspect and clean twice a y		
Alarms – Alarm signals when there is a pro		y time an alarm signals.
Event counter or water meter – Record you		
-recommend meter readings be co	onducted ( <i>circle one: <u>DAILY</u> <u>WE</u></i>	EEKLY MONTHLY)
Professional Management Tasks		
🕱 ' Check to make sure tank is not lea	king	
☐ Check and clean the in-tank effluer	nt filter	
	in all septic tanks	
🏿 Recommend if tank should be pum	iped	
☐ Check the drainfield effluent levels	in the rock layer	
☑ Check the pump and alarm system	functions	
图 Check wiring for corrosion and fund	ction	
Check dissolved oxygen and effluer	nt temperature in tank	
💢 Provide homeowner with list of res	sults and any action to be taken	
☐ Flush and clean laterals if cleanouts	s exist	RC
"I understand it is my responsibility to properly operate and main Management Plan. If requirements in the Management Plan are a necessary corrective actions. If I have a new system, I agree to ad system."	ntain the sewage treatment system on t not met, I will promptly notify the perm	itting authority and take
Property Owner Signature:	Date: _	
Designer Signature: Marke Minghing	Date: _	5/13/16

See Reverse Side for Management Log

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# **Maintenance Log**

Date Accomplished					
		<u>-</u> -			
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×.			2		
			Date Accompl		

P:\PZSHARE\Forms\SSTS Management Plan.docx

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