



Soderstrom Septic LLC.

6/18/2024

Greg Dorau

12405 State Hwy. 18

Finlayson, MN 55735

PID: 34-0-023700

I have completed the septic design for your home located at 12405 State Hwy. 18 Finlayson, in Wagner Township, Aitkin County.

I have sized the system for a 4-bedroom home with more than two water using appliances. The septic tank will be a 1,600-gallon septic tank, followed by a 1,000-gallon pump tank. The pump that is required for this system must have the ability to deliver 38 gpm with at least 17.55 feet of head. The soil treatment area will utilize a type III mound pressure distribution system.

Being a type III system, a monitoring and mitigation plan will need to be followed. Inspections will be required every 3, 6, 12, and 24 months. After the two-year time period if the system is operating correctly it may be signed off as operating effectively by a licensed professional. An event count meter will need to be installed on the pump tank side of the tank to monitor how much effluent is being dosed to the mound system.

The tank and mound area have been staked. The property lines will need to be verified that they are at least 10 feet from these stakes.

This system is designed for domestic septic waste from the home. Clean water from footing drains, water softening units, or furnaces must not enter this system.

I recommend to pump the septic and pump tank out every 2 years, and regularly mow the mound and tank area keeping them as part of your lawn. Thank you for your business, and I am sure you will be pleased with this new septic system.

Sincerely,

Angela Tvedt

Angela Tvedt

Soderstrom Septic LLC.

License #: 4146

Installation Notes

1. There are 2 existing systems that will need to be pumped out and properly abandoned.
2. The new septic tank will be a 1,600-gallon septic tank, followed by a 1,000-gallon pump tank.
3. A clean out will need to be installed just outside the house.
4. An event count meter will need to be installed on the pump line to monitor how much effluent is being dosed to the mound system.
5. The pump line will need to have a maintenance loop inside the pump tank for easier maintenance access that comes up within a foot of the bottom of the lid.
6. An outdoor pedestal with outlet and alarm will need to be installed, so an electrician can come and hook up the alarm and outlet for the pump and floats.
7. The mound will need to be built with 4:1 slope, so it can be mowed and maintained as part of the lawn.
8. Once the system is installed the site will need to be covered with topsoil and grass seeded.

FIELD EVALUATION SHEET

PRELIMINARY EVALUATION DATE 6/18/2024 , FIELD EVALUATION DATE 6/18/2024
PROPERTY OWNER: Greg Dorau PHONE 651-210-8415
ADDRESS: 12405 Hwy. 18 CITY, STATE, ZIP: Finlayson, MN 55735
LEGAL DESCRIPTION: NW of NE 40 acres
PIN# 34-0-023700 SEC 15 T 43 R 22 TWP NAME Wagner
FIRE# _____ LAKE/RIVER N/A LAKE CLASS N/A OHWL N/A FT. _____

DESCRIPTION OF SOIL TREATMENT AREAS

| | AREA #1 | AREA #2 | REFERENCE BM ELEV. <u>100</u> FT. |
|--------------------|---------------------|-----------------------|-----------------------------------|
| DISTURBED AREAS | YES ___ NO <u>x</u> | YES ___ NO <u>N/A</u> | REFERENCE BM DESCRIPTION _____ |
| COMPACTED AREAS | YES ___ NO <u>x</u> | YES ___ NO <u>N/A</u> | <u>transit by pump tank</u> |
| FLOODING | YES ___ NO <u>x</u> | YES ___ NO <u>N/A</u> | _____ |
| RUN ON POTENTIAL | YES ___ NO <u>x</u> | YES ___ NO <u>N/A</u> | _____ |
| SLOPE % | <u>1.5</u> | <u>N/A</u> | _____ |
| DIRECTION OF SLOPE | <u>SE</u> | <u>N/A</u> | _____ |
| LANDSCAPE POSITION | <u>Footslope</u> | _____ | _____ |
| VEGETATION TYPES | <u>Grass</u> | _____ | _____ |

DEPTH TO STANDING WATER OR MOTTLED SOIL: BORING# 1 3" , 1A 3" , 2 3" , 2A 3"

BOTTOM ELEVATION-FIRST TRENCH OR BOTTOM OF ROCK BED: #1 103 FT., #2 N/A FT.

SOIL SIZING FACTOR: SITE #1 .5 , SITE #2 N/A

CONSTRUCTION RELATED ISSUES: there is an existing system to abandon

LIC# 4146 SITE EVALUATOR SIGNATURE: Angela Tvedt

SITE EVALUATOR NAME: Angela Tvedt TELEPHONE# 320-515-1081

LUG REVIEW _____ DATE _____

Comments: _____

SOIL BORING LOGS ON REVERSE SIDE

SOILS CHARTS FOR BOTH PROPOSED AND ALTERNATE SITES

1 (PROPOSED) SOILS DATA

| DEPTH (INCHES) | TEXTURE | MUNSELL COLOR |
|-------------------|--|------------------|
| 0 - 5" | Siltloam | 10YR 3/2 |
| 3" | Siltloam | 10YR 3/2 |
| | 10YR 6/3 Depletion 10YR 5/8 Concentration | |

2 (PROPOSED) SOILS DATA

| DEPTH (INCHES) | TEXTURE | MUNSELL COLOR |
|-------------------|--|------------------|
| 0 - 5" | Siltloam | 10YR 3/2 |
| 3" | Siltloam | 10YR 3/2 |
| | 10YR 6/3 Depletion 10YR 5/8 Concentration | |

1 (ALTERNATE) SOILS DATA

| DEPTH (INCHES) | TEXTURE | MUNSELL COLOR |
|-------------------|---------|------------------|
| | | |

2 (ALTERNATE) SOILS DATA

| DEPTH (INCHES) | TEXTURE | MUNSELL COLOR |
|-------------------|---------|------------------|
| | | |

ADDITIONAL SOIL BORINGS MAY BE REQUIRED

MOUND DESIGN WORK SHEET (For Flows up to 1200 gpd)

A. Average Design FLOW

Estimated 600 gpd (see figure A-1)
 or measured _____ x 1.5 (safety factor) = _____ gpd

A-1: Estimated Sewage Flows in Gallons per Day

| number of bedrooms | Class I | Class II | Class III | Class IV |
|--------------------|---------|----------|-----------|------------|
| 2 | 300 | 225 | 180 | 60% |
| 3 | 450 | 300 | 218 | of the |
| 4 | 600 | 375 | 256 | values |
| 5 | 750 | 450 | 294 | in the |
| 6 | 900 | 525 | 332 | Class I, |
| 7 | 1050 | 600 | 370 | II, or III |
| 8 | 1200 | 675 | 408 | columns. |

B. SEPTIC TANK Capacity

1,600 gallons (see figure C-1)

C-1: Septic Tank Capacities (in gallons)

| Number of Bedrooms | Minimum Liquid Capacity | Liquid capacity with garbage disposal | Liquid capacity with disposal & lift inside |
|--------------------|-------------------------|---------------------------------------|---|
| 2 or less | 750 | 1125 | 1500 |
| 3 or 4 | 1000 | 1500 | 2000 |
| 5 or 6 | 1500 | 2250 | 3000 |
| 7, 8 or 9 | 2000 | 3000 | 4000 |

C. SOILS (refer to site evaluation)

- Depth to restricting layer = .25 feet
- Depth of percolation tests = N/A feet
- Texture Siltloam
 Percolation rate N/A mpi
- Soil loading rate .5 gpd/sqft (see figure D-33)
- Percent land slope 1.5 %

D. ROCK LAYER DIMENSIONS

- Multiply average design flow (A) by 0.83 to obtain required rock layer area.
600 gpd x 0.83 sqft/gpd = 500 sqft
- Determine rock layer width = 0.83 sqft/gpd x linear Loading Rate (LLR)
 0.83 sqft/gpd x 12 gpd/sqft = 10 ft
- Length of rock layer = area ÷ width =
500 sqft (D1) ÷ 10 ft (D2) = 50 ft

Mound LLR

< 120 MPI ≤ 12
 ≥ 120 MPI ≤ 6

E. ROCK VOLUME

- Multiply rock area (D1) by rock depth of 1 ft to get cubic feet of rock
500 sqft x 1 ft = 500 cuft
- Divide cuft by 27 cuft/cuyd to get cubic yards
500 cuft ÷ 27 cuyd/cuft = 18.5 cuyd
- Multiply cubic yards by 1.4 to get weight of rock in tons
18.5 cuyd x 1.4 ton/cuyd = 25.9 tons

F. SEWAGE ABSORPTION WIDTH

Absorption width equals absorption ratio (See Figure D-33)
 times rock layer width (D2)

2.4 x 10 ft = 24 ft

D-33: Absorption Width Sizing Table

| Percolation Rate in Minutes per Inch (MPI) | Soil Texture | Loading Rate Gallons per day per square foot | Absorption Ratio |
|--|---|--|------------------|
| Faster than 5 | Coarse Sand Medium Sand Loamy Sand Fine Sand | 1.20 | 1.00 |
| 5 to 15 | Sandy Loam | 0.75 | 1.20 |
| 16 to 30 | Loam | 0.60 | 2.00 |
| 31 to 45 | Silt Loam Silt | 0.50 | 2.40 |
| 46 to 60 | Sandy Clay Loam Silty Clay Loam Clay Loam | 0.45 | 2.67 |
| 61 to 120 | Silty Clay Sandy Clay Clay | 0.24 | 5.00 |
| Slower than 120* | | | |

*System designed for these soils must be other or performance

G. MOUND SLOPE WIDTH & LENGTH

(landslope greater than 1%)

1. Downslope absorption width = absorption width (F)

minus rock layer width (D2)

$24 \text{ ft} - 10 \text{ ft} = 14 \text{ ft}$

2. Calculate mound size

UPSLOPE

a. Depth of clean sand fill at upslope edge of

rock layer = 3 ft minus the distance to restricting layer (C1)

$3 \text{ ft} - 0 \text{ ft} = 3 \text{ ft}$

b. Mound height at the upslope edge of rock layer = depth of clean sand for separation (G2a)

at upslope edge plus depth of rock layer (1 ft)

plus depth of cover (1 ft)

$3 \text{ ft} + 1 \text{ ft} + 1 \text{ ft} = 5 \text{ ft}$

c. Upslope berm multiplier based on land slope

$\frac{3.70}{3.70}$ (see figure D-34)

d. Upslope width = berm multiplier (G2c) x upslope mound height (G2b):

$3.70 \times 5 \text{ ft} = 18.5 \text{ ft}$

DOWNSLOPE

e. Drop in elevation = rock layer width (D2) x percent landslope (C5) ÷ 100

$10 \text{ ft} \times 1.5 \% \div 100 = .15 \text{ ft}$

f. Downslope mound height = depth of clean sand for slope difference (G2e) at downslope rock edge plus the mound height at the upslope edge of rock layer (G2b)

$5 \text{ ft} + .15 \text{ ft} = 5.15 \text{ ft}$

g. Downslope berm multiplier based on percent land slc.

$\frac{4.35}{4.35}$ (see figure D-34)

h. Downslope width = downslope multiplier (G2g) times downslope mound height (G2f)

$4.35 \times 5.15 \text{ ft} = 22.4 \text{ ft}$

i. Select the greater of G1 and G2h as the downslope width: 22.4 ft

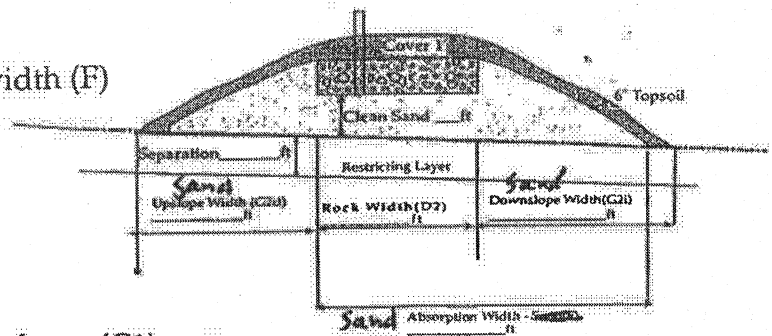
j. Total mound width is the sum of upslope width (G2d) width plus rock layer width (D2) plus downslope width (G2i)

$18.5 \text{ ft} + 10 \text{ ft} + 22.4 \text{ ft} = 50.9 \text{ ft}$

k. Total mound length is the sum of upslope width (G2d) plus rock layer length (D3) plus upslope width (G2d)

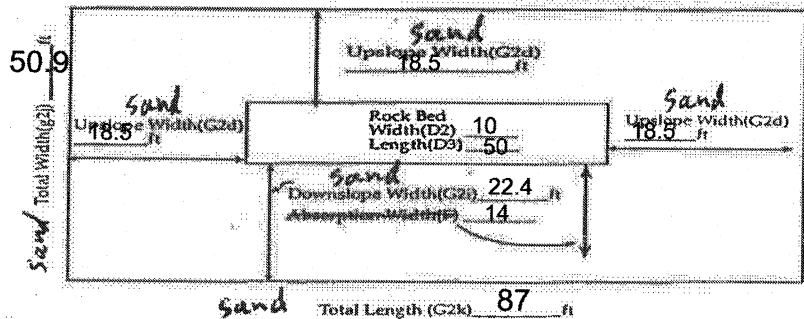
$18.5 \text{ ft} + 50 \text{ ft} + 18.5 \text{ ft} = 87 \text{ feet}$

Landslope > 1% slope



D-34: SLOPE MULTIPLIER TABLE

| Land Slope in % | UPSLOPE multipliers for various slope ratios | | | | | | DOWNSLOPE multipliers for various slope ratios | | | | |
|-----------------|--|------|------|------|------|------|--|------|-------|-------|-------|
| | 3:1 | 4:1 | 5:1 | 6:1 | 7:1 | 8:1 | 3:1 | 4:1 | 5:1 | 6:1 | 7:1 |
| 0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 |
| 1 | 2.91 | 3.85 | 4.76 | 5.66 | 6.54 | 7.41 | 3.09 | 4.17 | 5.26 | 6.38 | 7.53 |
| 2 | 2.83 | 3.70 | 4.54 | 5.36 | 6.14 | 6.90 | 3.19 | 4.35 | 5.56 | 6.82 | 8.14 |
| 3 | 2.75 | 3.57 | 4.35 | 5.08 | 5.79 | 6.45 | 3.30 | 4.54 | 5.88 | 7.32 | 8.86 |
| 4 | 2.68 | 3.45 | 4.17 | 4.84 | 5.46 | 6.06 | 3.41 | 4.76 | 6.25 | 7.89 | 9.72 |
| 5 | 2.61 | 3.33 | 4.00 | 4.62 | 5.19 | 5.71 | 3.53 | 5.00 | 6.67 | 8.57 | 10.77 |
| 6 | 2.54 | 3.23 | 3.85 | 4.41 | 4.93 | 5.41 | 3.66 | 5.26 | 7.14 | 9.38 | 12.07 |
| 7 | 2.48 | 3.12 | 3.70 | 4.23 | 4.70 | 5.13 | 3.80 | 5.56 | 7.69 | 10.34 | 13.73 |
| 8 | 2.42 | 3.03 | 3.57 | 4.05 | 4.49 | 4.88 | 3.95 | 5.88 | 8.33 | 11.54 | 15.91 |
| 9 | 2.36 | 2.94 | 3.45 | 3.90 | 4.30 | 4.65 | 4.11 | 6.25 | 9.09 | 13.04 | 18.92 |
| 10 | 2.31 | 2.86 | 3.33 | 3.75 | 4.12 | 4.44 | 4.29 | 6.67 | 10.00 | 15.00 | 23.33 |
| 11 | 2.26 | 2.78 | 3.23 | 3.61 | 3.95 | 4.26 | 4.48 | 7.14 | 11.11 | 17.65 | 30.43 |
| 12 | 2.21 | 2.70 | 3.12 | 3.49 | 3.80 | 4.08 | 4.69 | 7.69 | 12.50 | 21.43 | 43.75 |



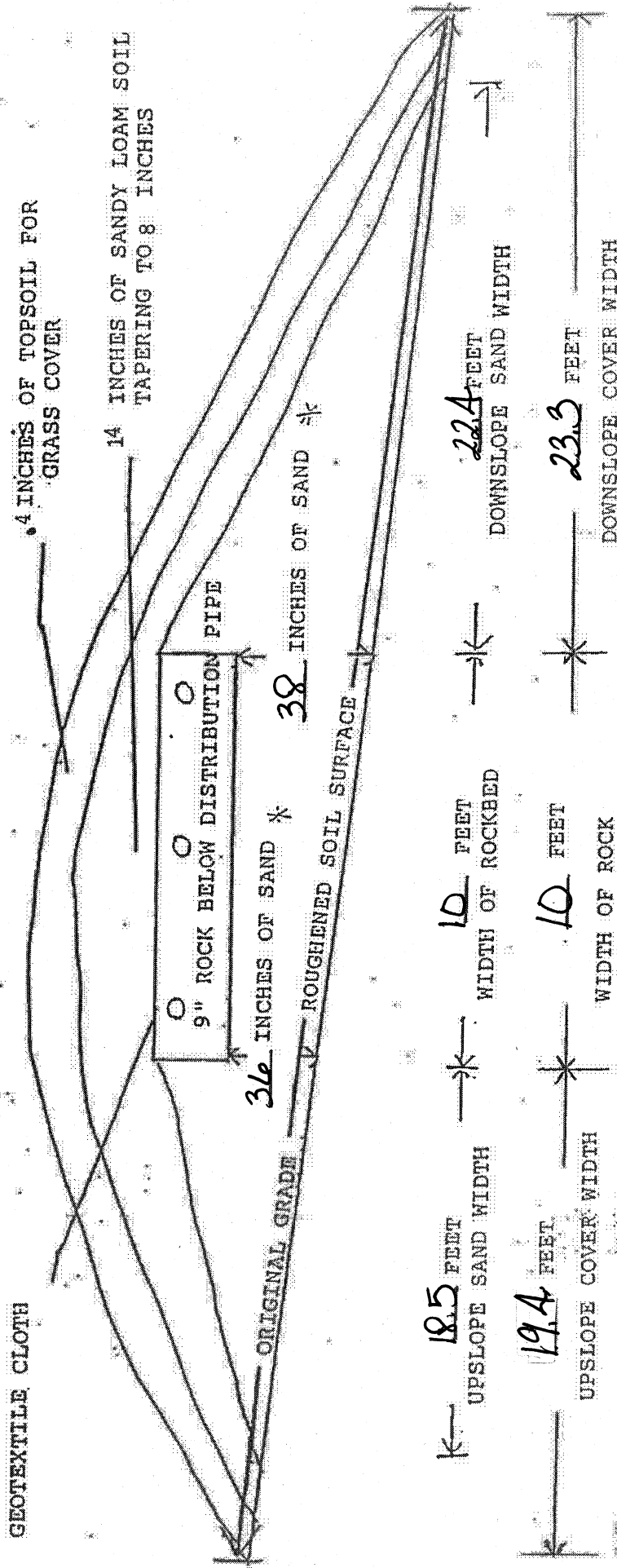
Final Dimensions:
50.9 X 87

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Angela Tvedt (signature) 4146 (license #) 6/18/2024 (date)

OUND CROSS-SECTION

1.5 PERCENT SLOPE OF ORIGINAL SOIL
10 FT. X 50 FT. SIZE OF ROCKBED 24 FT. X 50 FT. SIZE OF SANDBASE



PRESSURE DISTRIBUTION SYSTEM

- Select number of perforated laterals 3
- Select perforation spacing = 3 ft
- Since perforations should not be placed closer than 1 foot to the edge of the rock layer (see diagram), subtract 2 feet from the rock layer length.

$$\frac{50}{\text{Rock layer length}} - 2 \text{ ft} = \underline{48} \text{ ft}$$

- Determine the number of spaces between perforations. Divide the length (3) by perforation spacing (2) and round down to nearest whole number.

$$\text{Perforation spacing} = \underline{48} \text{ ft} \div \underline{3} \text{ ft} = \underline{16} \text{ spaces}$$

- Number of perforations is equal to one plus the number of perforation spaces(4). Check figure E-4 to assure the number of perforations per lateral guarantees <10% discharge variation.

$$\underline{16} \text{ spaces} + 1 = \underline{17} \text{ perforations/lateral}$$

- A. Total number of perforations = perforations per lateral (5) times number of laterals (1)

$$\underline{17} \text{ perfs/lat} \times \underline{3} \text{ lat} = \underline{51} \text{ perforations}$$

- B. Calculate the square footage per perforation. Should be 6-10 sqft/perf. Does not apply to at-grades.

Rock bed area = rock width (ft) x rock length (ft)

$$\underline{10} \text{ ft} \times \underline{50} \text{ ft} = \underline{500} \text{ sqft}$$

Square foot per perforation = Rock bed area ÷ number of perfs (6)

$$\underline{500} \text{ sqft} \div \underline{51} \text{ perfs} = \underline{9.8} \text{ sqft/perf}$$

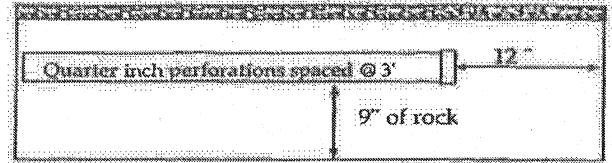
- Determine required flow rate by multiplying the total number of perforations (6A) by flow per perforation (see figure E-6)

$$\underline{51} \text{ perfs} \times \underline{.74} \text{ gpm/perfs} = \underline{37.74} \text{ gpm}$$

- If laterals are connected to header pipe as shown on upper example, to select minimum required lateral diameter; enter figure E-4 with perforation spacing (2) and number of perforations per lateral (5) Select minimum diameter for perforated lateral = 2 inches.

- If perforated lateral system is attached to manifold pipe near the center, lower diagram, perforated lateral length (3) and number of perforations per lateral (5) will be approximately one half of that in step 8. Using these values, select minimum diameter for perforated lateral = _____ inches.

Geotextile fabric



Perf Sizing 3/16" - 1/4"
Perf Spacing 1.5'- 5'

E-4: Maximum allowable number of 1/4-inch perforations per lateral to guarantee <10% discharge variation

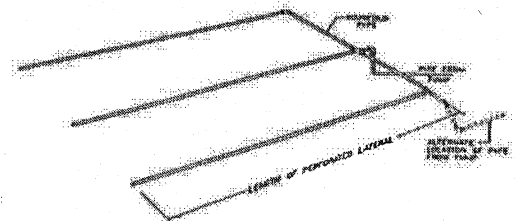
| perforation spacing (feet) | 1 inch | 1.25 inch | 1.5 inch | 2.0 inch |
|----------------------------|--------|-----------|----------|----------|
| 2.5 | 8 | 14 | 18 | 28 |
| 3.0 | 8 | 13 | 17 | 26 |
| 3.3 | 7 | 12 | 16 | 25 |
| 4.0 | 7 | 11 | 15 | 23 |
| 5.0 | 6 | 10 | 14 | 22 |

E-6: Perforation Discharge in gpm

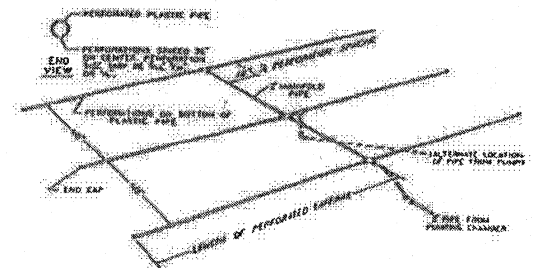
| head (feet) | perforation diameter (inches) | | | |
|------------------|-------------------------------|------|------|------|
| | 1/8 | 3/16 | 7/32 | 1/4 |
| 1.0 ^a | 0.18 | 0.42 | 0.56 | 0.74 |
| 2.0 ^b | 0.26 | 0.59 | 0.80 | 1.04 |
| 5.0 | 0.41 | 0.94 | 1.26 | 1.65 |

^a Use 1.0 foot for single-family homes.
^b Use 2.0 feet for anything else.

MANIFOLD LOCATED AT END OF PRESSURE DISTRIBUTION SYSTEM



LAYOUT OF PERFORATED PIPE LATERALS FOR PRESSURE DISTRIBUTION IN MOUND



I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Angela Tvedt

(signature)

4146

(license #)

6/18/2024

(date)

PUMP SELECTION PROCEDURE

1. Determine pump capacity:

A. Gravity distribution

1. Minimum required discharge is 10 gpm
2. Maximum suggested discharge is 45 gpm. For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device.

B. Pressure distribution

See pressure distribution work sheet

From A or B Selected pump capacity: 38 gpm

2. Determine pump head requirements:

A. Elevation difference between pump and point of discharge?

11.2 feet

B. Special head requirement? (See Figure at right - Special Head Requirements)

5 feet

C. Calculate Friction loss

1. Select pipe diameter 2 in

2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1).

Read friction loss in feet per 100 feet from Figure E-9

Friction Loss = 2.64 ft/100ft of pipe

3. Determine total pipe length from pump discharge to soil treatment discharge point. Estimate by adding 25 percent to pipe length for fitting loss. Total pipe length times 1.25 = equivalent pipe length

41 feet x 1.25 = 51.25 feet

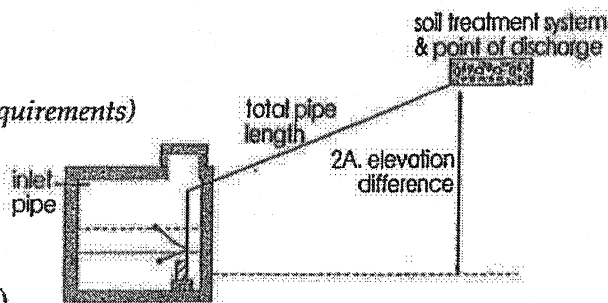
4. Calculate total friction loss by multiplying friction loss (C2) in ft/100 ft by the equivalent pipe length (C3) and divide by 100.

= 2.64 ft/100ft x 51.25 ÷ 100 = 1.35 ft

D. Total head required is the sum of elevation difference (A), special head requirements (B), and total friction loss (C4)

11.2 ft + 5 ft + 1.35 ft =

Total head: 17.55 feet



| Special Head Requirements | |
|---------------------------|------|
| Gravity Distribution | 0 ft |
| Pressure Distribution | 5 ft |

| E-9: Friction Loss in Plastic Pipe | | | |
|------------------------------------|--------------------------|------|------|
| Per 100 feet | | | |
| flow rate gpm | nominal pipe diameter | | |
| | 1.5" | 2" | 3" |
| 20 | 2.47 | 0.73 | 0.11 |
| 25 | 3.73 | 1.11 | 0.16 |
| 30 | 5.23 | 1.55 | 0.23 |
| 35 | 6.96 | 2.06 | 0.30 |
| 40 | 8.91 | 2.64 | 0.39 |
| 45 | 11.07 | 3.28 | 0.48 |
| 50 | 13.46 | 3.99 | 0.58 |
| 55 | | 4.76 | 0.70 |
| 60 | | 5.60 | 0.82 |
| 65 | | 6.48 | 0.95 |
| 70 | | 7.44 | 1.09 |

3. Pump selection

A pump must be selected to deliver at least 38 gpm (1A or B) with at least 17.55 feet of total head (2D)

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Angela Tvedt (signature) 4146 (license #) 6/18/2024 (date)

DOSING CHAMBER SIZING

1. Determine area

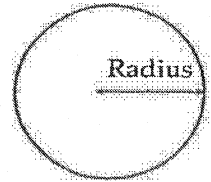
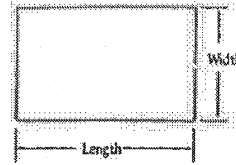
A. Rectangle area = L x W

_____ x _____ = _____ square feet

B. Circle area = π (3.14) x radius in feet x radius in feet

3.14 x _____ ft x _____ ft = _____ sqft

C. Get area from manufacturer _____ sqft



2. Calculate gallons per inch

There are 7.5 gallons per cubic foot of volume, therefore multiply the area (1A, B or C) times the conversion factor and divide by 12 inches per foot to calculate gallon per inch.

Area x 7.5 ÷ 12 = _____ sqft x 7.5 ÷ 12 in/ft = 23 gallon per inch

3. Calculate total tank volume

A. Depth from bottom of inlet pipe to tank bottom 44 in

B. Total tank volume = depth from bottom of inlet pipe to tank bottom (3A) x gal/in (2)
= 44 in x 23 gal/in = 1012 gal

Legal Tank:
500 gallons or
100% the Daily flow
or
Alternating Pumps

4. Calculate gallons to cover pump (with 2-3 inches of water covering pump)

(Pump and block height (inch) + 2 inch) x gallon/inch

(4 in + 2 in) x 23 gal/in = 138 gallon

| number of bedrooms | Class I | Class II | Class III | Class IV |
|--------------------|---------|----------|-----------|------------|
| 2 | 300 | 225 | 180 | 60% |
| 3 | 450 | 300 | 218 | of the |
| 4 | 600 | 375 | 256 | volumes |
| 5 | 750 | 450 | 294 | in the |
| 6 | 900 | 525 | 332 | Class I, |
| 7 | 1050 | 600 | 370 | II, or III |
| 8 | 1200 | 675 | 408 | columns. |

5. Calculate total pumpout volume

A. Select pump size for 4-5 does per day. Gallon per dose = gpd (see figure A-1)
/ doses per day = 600 gpd ÷ 5 doses/day = 120 gallons

B. Calculate drainback

1. Determine total pipe length, 41 feet

2. Determine liquid volume of pipe, 0.17 gal per ft (see figure E-20)

3. Drainback quantity = 41 ft (5B1) x 0.17 gal per ft (5B2) = 6.97 gal

C. Total pump out volume = dose volume (5A) + drainback (5B3)
120 gal + 6.97 gal = 126.97 Total gallon

| Pipe Diameter inches | Gallons per foot |
|----------------------|------------------|
| 1 | 0.045 |
| 1.25 | 0.078 |
| 1.5 | 0.11 |
| 2 | 0.17 |
| 2.5 | 0.25 |
| 3 | 0.38 |
| 4 | 0.66 |

6. Float separation distance (using total pumpout volume)

Total pumpout volume (5C) ÷ gal/inch (2)

126.97 gal ÷ 24 gal/in = 5.29 inch

7. Calculate volume for alarm (typically 2 to 3 inches)

Alarm depth (inch) x gallon/inch (2) = 3 in x 23 gal/in = 69 gal

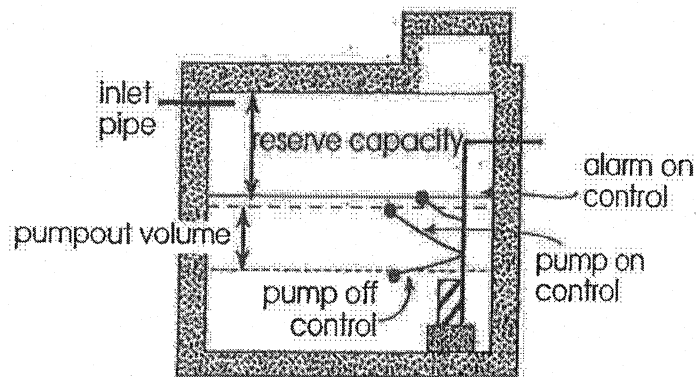
8. Calculate total gallon = gallons over pump (4) + gallons pumpout (5C) + gallons alarm (7)

138 gal + 126.97 gal + 69 gal = 333.97 gallons

9. Total Tank Depth = total gallon (8) ÷ gallon/inch (2)

333.97 gal ÷ 23 gal/in = 14.5 in

Recommended:
Calculate reserve capacity (75% the daily flow)
Daily flow x .75 = 600 x .75 = 450 gallons



I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

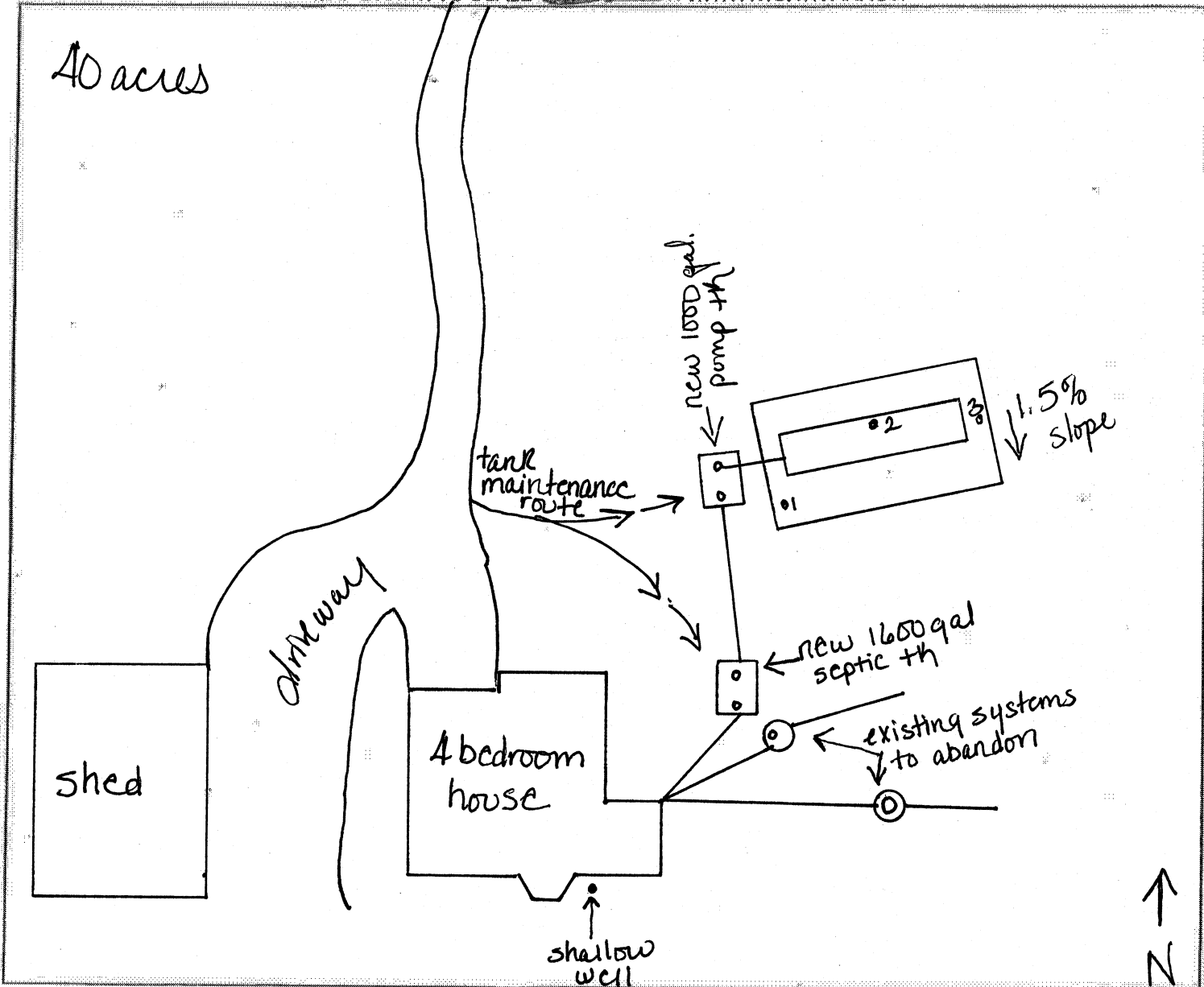
Angela Tvedt (signature) 4146 (license #) 6/18/24 (date)

SKETCH SHEET

CLIENT: Greg Doran

DATE: 6/18/24

MAP DRAWN TO SCALE WITH A NORTH ARROW



CHECK OFF LIST - HAVE ALL OF THE FOLLOWING BEEN DRAWN ON THE MAP??

SHOW EXISTING OR PROPOSED

- WATER WELLS WITHIN 100 FT OF TREATMENT AREAS
- PRESSURE WATER LINES WITHIN 10 FT OF TREATMENT AREAS
- STRUCTURES
- LOT IMPROVEMENTS
- ALL SOIL TREATMENT AREAS
- ALL LISTS COMPONENTS
- HORIZONTAL AND VERTICAL REFERENCE
- POINT OF SOIL BORINGS
- DIRECTION OF SLOPE
- LOT EASEMENTS
- ALL LOT DIMENSIONS
- DISTURBED/COMPACTED AREAS
- SITE PROTECTION - LATHE AND RIBBON EVERY 15 FT
- ACCESS ROUTE FOR TANK MAINTENANCE

REQUIRED SETBACKS

- STRUCTURES
- PROPERTY LINES
- CHWL

COMMENTS:

INDICATE ELEVATIONS

- BENCHMARK 100-59"
- ELEVATION OF SEWER LINE @ HOUSE 100
- ELEVATION @ TANK INLET 99
- ELEVATION @ BOTTOM OF ROCK LAYER 103.5
- ELEVATION @ BOTTOM OF BORING OR RESTRICTIVE LAYER 100
- ELEVATION OF PUMP 93
- ELEVATION OF DISTRIBUTION DEVICE 103.5

DESIGNER SIGNATURE Angela Tvedt
 LICENSE# 4146

DATE 6/18/24

