

Subsurface Sewage Treatment System Management Plan

Property Owner: Dale Volter
Mailing Address: 190 Grove RD
Site Address: 28796 220th ST

Phone: 612-718-6365 Date: 4-15-2024
City: East Bethel Zip: 55092
City: Isle Zip: 56347

This management plan will identify the operation and maintenance activities necessary to ensure long-term performance of your septic system. Some of these activities must be performed by you, the homeowner. Other tasks must be performed by a licensed septic service provider or maintenance provider.

System Designer: Recommends SSTS check every 36 months.
Local Government: Recommends SSTS check every 36 months.
State Requirement: Requires SSTS check every 36 months.
(State requirements are based on MN Rules Chapter 7080.2450, Subp. 2 & 3)

My System needs to be checked every 36 months.

Homeowner Management Tasks:

- Leaks – Check (look, listen) for leaks in toilets and dripping faucets. Repair leaks promptly.
- Surfacing sewage – Regularly check for wet or spongy soil around your soil treatment area.
- Effluent filter – *Inspect and clean twice a year or more.*
- Alarms – Alarm signals when there is a problem. Contact a service or maintenance provider any time an alarm signals.
- Event counter or water meter – Record your water use.
-recommend meter readings be conducted (circle one: DAILY WEEKLY MONTHLY N/A)

Licensed septic service provider or maintenance provider (Check all that apply):

- Check to make sure tank is not leaking
- Check and clean the in-tank effluent filter (if exists)
- Check the sludge/scum layer levels in all septic tanks
- Recommend if tank should be pumped
- Check inlet and outlet baffles
- Check the drainfield effluent levels in the rock layer
- Check the pump and alarm system functions
- Check wiring for corrosion and function
- Check dissolved oxygen and effluent temperature in tank
- Provide homeowner with list of results and any action to be taken
- Flush and clean laterals if cleanouts exist

"I understand it is my responsibility to properly operate and maintain the sewage treatment system on this property, utilizing the Management Plan. If requirements in the Management Plan are not met, I will promptly notify the permitting authority and take necessary corrective actions. If I have a new system, I agree to adequately protect the reserve area for future use as a soil treatment system."

Property Owner Signature: Dale Volter Date: 4/2024
Designer Signature: Dave Eydahl Date: 4/17/2024

See Reverse Side for Management Log

FIELD EVALUATION SHEET

PRELIMINARY EVALUATION DATE 4/12/2024, FIELD EVALUATION DATE 4/12/2024
PROPERTY OWNER: Dave Voltin PHONE 612-718-6565
ADDRESS: 28796 220th St. CITY, STATE, ZIP: _____
LEGAL DESCRIPTION: _____
PIN# 210-058200 SEC 36 T 460 R 25 TWP NAME MALMO
FIRE# --- LAKE/RIVER --- LAKE CLASS --- OHWL --- FT.

DESCRIPTION OF SOIL TREATMENT AREAS

	AREA #1	AREA #2	REFERENCE BM ELEV. <u>180</u> FT
DISTURBED AREAS	YES <u>---</u> NO <u>X</u>	YES <u>---</u> NO <u>---</u>	REFERENCE BM DESCRIPTION <u>---</u>
COMPACTED AREAS	YES <u>---</u> NO <u>X</u>	YES <u>---</u> NO <u>---</u>	<u>Top of ELEC. TRANSFORMER</u>
FLOODING	YES <u>---</u> NO <u>X</u>	YES <u>---</u> NO <u>---</u>	_____
RUN ON POTENTIAL	YES <u>---</u> NO <u>X</u>	YES <u>---</u> NO <u>---</u>	_____
SLOPE %	<u>1%</u>	_____	_____
DIRECTION OF SLOPE	<u>South</u>	_____	_____
LANDSCAPE POSITION	<u>Summit</u>	_____	_____
VEGETATION TYPES	<u>Paper Birch</u>	_____	_____

DEPTH TO STANDING WATER OR MOTTLED SOIL: BORING# 1 18", 1A 18", 2 ---, 2A ---

BOTTOM ELEVATION--FIRST TRENCH OR BOTTOM OF ROCK BED: #1 +18 FT., #2 --- FT.

SOIL SIZING FACTOR: ~~SITE #1 1167~~, SITE #2 1167

CONSTRUCTION RELATED ISSUES: _____

LIC# 62006 SITE EVALUATOR SIGNATURE: Dave Engdahl

SITE EVALUATOR NAME: Dave Engdahl TELEPHONE# 320-592-3606

LUG REVIEW _____ DATE _____

Comments: _____

SOIL BORING LOGS ON REVERSE SIDE

MOUND DESIGN WORK SHEET (For Flows up to 1200 gpd)

A. Average Design FLOW

Estimated 300 gpd (see figure A-1)
 or measured x 1.5 (safety factor) = gpd

number of bedrooms	Class I	Class II	Class III	Class IV
2	300	225	180	60%
3	450	300	218	of the
4	600	375	256	values
5	750	450	294	in the
6	900	525	332	Class I,
7	1050	600	370	II, or III
8	1200	675	408	columns.

B. SEPTIC TANK Capacity

1000 gallons (see figure C-1)

C. SOILS (refer to site evaluation)

- Depth to restricting layer = 1.5 feet
- Depth of percolation tests = feet
- Texture Fine Sand Loam
 Percolation rate 1.67/20 mpi
- Soil loading rate 60 gpd/sqft (see figure D-33)
- Percent land slope 1 %

Number of Bedrooms	Minimum Liquid Capacity	Liquid capacity with garbage disposal	Liquid capacity with disposal & lift inside
2 or less	750	1125	1500
3 or 4	1000	1500	2000
5 or 6	1500	2250	3000
7, 8 or 9	2000	3000	4000

D. ROCK LAYER DIMENSIONS

- Multiply average design flow (A) by 0.83 to obtain required rock layer area.
300 gpd x 0.83 sqft/gpd = 250 sqft
- Determine rock layer width = 0.83 sqft/gpd x linear Loading Rate (LLR)
 0.83 sqft/gpd x 12 gpd/sqft = 10 ft
- Length of rock layer = area ÷ width =
250 sqft (D1) ÷ 10 ft (D2) = 25 ft

< 120 MPI	≤ 12
≥ 120 MPI	≤ 6

E. ROCK VOLUME

- Multiply rock area (D1) by rock depth of 1 ft to get cubic feet of rock
250 sqft x 1 ft = 250 cuft
- Divide cuft by 27 cuft/cuyd to get cubic yards
250 cuft ÷ 27 cuft/cuyd = 9.3 cuyd
- Multiply cubic yards by 1.4 to get weight of rock in tons
9.3 cuyd x 1.4 ton/cuyd = 13.02 tons

F. SEWAGE ABSORPTION WIDTH

Absorption width equals absorption ratio (See Figure D-33) times rock layer width (D2)

10 x 2.0 ft = 20 ft

Percolation Rate in Minutes per Inch (MPI)	Soil Texture	Loading Rate Gallons per day per square foot	Absorption Ratio
Faster than 5	Coarse Sand Medium Sand Loamy Sand Fine Sand	1.20	1.00
6 to 15	Sandy Loam	0.72	1.50
16 to 30	Loam	0.60	2.00
31 to 45	Silt Loam	0.50	2.40
46 to 60	Silt Sandy Clay Loam Silty Clay Loam Clay Loam	0.45	2.67
61 to 120	Silty Clay Sandy Clay Clay	0.24	5.00
Slower than 120*			

*System designed for these soils must be other or performance

G. MOUND SLOPE WIDTH & LENGTH

(landslope greater than 1%)

1. Downslope absorption width = absorption width (F)

minus rock layer width (D2)

$20 \text{ ft} - 10 \text{ ft} = 10 \text{ ft}$

2. Calculate mound size

UPSLOPE

a. Depth of clean sand fill at upslope edge of rock layer = 3 ft minus the distance to restricting layer (C1)

$3 \text{ ft} - 1.5 \text{ ft} = 1.5 \text{ ft}$

b. Mound height at the upslope edge of rock layer = depth of clean sand for separation (G2a) at upslope edge plus depth of rock layer (1 ft) plus depth of cover (1 ft)

$1.5 \text{ ft} + 1 \text{ ft} + 1 \text{ ft} = 3.5 \text{ ft}$

c. Upslope berm multiplier based on land slope

using 4.0 (see figure D-34)

d. Upslope width = berm multiplier (G2c) x upslope mound height (G2b):

$4.0 \times 3.5 \text{ ft} = 14 \text{ ft}$

DOWNSLOPE

e. Drop in elevation = rock layer width (D2) x percent landslope (C5) ÷ 100

$10 \text{ ft} \times 1 \% \div 100 = .1 \text{ ft}$

f. Downslope mound height = depth of clean sand for slope difference (G2e) at downslope

rock edge plus the mound height at the upslope edge of rock layer (G2b)

$3.5 \text{ ft} + .1 \text{ ft} = 3.6 \text{ ft}$

g. Downslope berm multiplier based on percent land slope

4.17 (see figure D-34)

h. Downslope width = downslope multiplier (G2g) times downslope mound height (G2f)

$4.17 \times 3.6 \text{ ft} = 15.0 \text{ ft}$

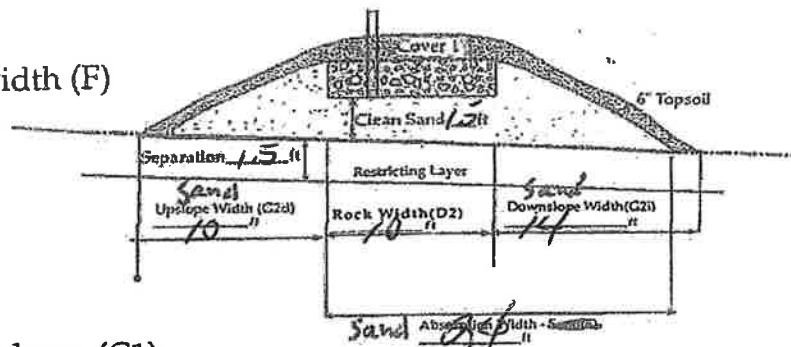
i. Select the greater of G1 and G2h as the downslope width: 15.0 ft

j. Total mound width is the sum of upslope width (G2d) width plus rock layer width (D2) plus downslope width (G2i)

$14.0 \text{ ft} + 10 \text{ ft} + 15.0 \text{ ft} = 39.0 \text{ ft}$

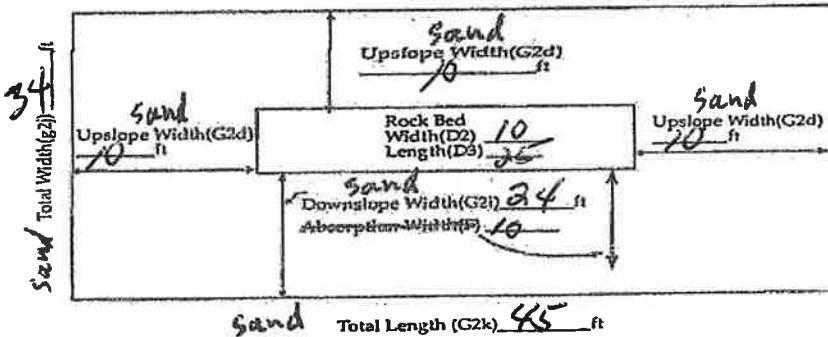
k. Total mound length is the sum of upslope width (G2d) plus rock layer length (D3) plus upslope width (G2d)

$14.0 \text{ ft} + 25 \text{ ft} + 14.0 \text{ ft} = 53.0 \text{ feet}$



D-34: SLOPE MULTIPLIER TABLE

Land Slope in %	UPSLOPE multipliers for various slope ratios						DOWNSLOPE multipliers for various slope ratios				
	3:1	4:1	5:1	6:1	7:1	8:1	3:1	4:1	5:1	6:1	7:1
0	3.0	4.0	5.0	6.0	7.0	8.0	3.0	4.0	5.0	6.0	7.0
1	2.91	3.85	4.76	5.66	6.54	7.41	3.09	4.17	5.26	6.38	7.53
2	2.83	3.70	4.54	5.36	6.14	6.90	3.19	4.35	5.56	6.82	8.14
3	2.75	3.57	4.35	5.08	5.79	6.45	3.30	4.54	5.88	7.32	8.86
4	2.68	3.45	4.17	4.84	5.46	6.06	3.41	4.76	6.25	7.89	9.72
5	2.61	3.33	4.00	4.62	5.19	5.71	3.53	5.00	6.67	8.57	10.77
6	2.54	3.23	3.85	4.41	4.93	5.41	3.66	5.26	7.14	9.38	12.07
7	2.48	3.12	3.70	4.23	4.70	5.13	3.80	5.56	7.69	10.34	13.73
8	2.42	3.03	3.57	4.05	4.49	4.88	3.95	5.88	8.33	11.54	15.91
9	2.36	2.94	3.45	3.90	4.30	4.65	4.11	6.25	9.09	13.04	18.92
10	2.31	2.86	3.33	3.75	4.12	4.44	4.29	6.67	10.00	15.00	23.33
11	2.26	2.78	3.23	3.61	3.95	4.26	4.48	7.14	11.11	17.65	30.43
12	2.21	2.70	3.12	3.49	3.80	4.08	4.69	7.69	12.50	21.43	43.75



Final Dimensions:
39 x 53

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Bruce E. Spalding (signature) LC2006 (license #) 4/17/2024 (date)

PUMP SELECTION PROCEDURE

1. Determine pump capacity:

A. Gravity distribution

1. Minimum required discharge is 10 gpm
2. Maximum suggested discharge is 45 gpm. For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device.

B. Pressure distribution

See pressure distribution work sheet

From A or B Selected pump capacity: 22.2 gpm

2. Determine pump head requirements:

A. Elevation difference between pump and point of discharge?

7 feet

B. Special head requirement? (See Figure at right - Special Head Requirements)

5 feet

C. Calculate Friction loss

1. Select pipe diameter 2" in

2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1).

Read friction loss in feet per 100 feet from Figure E-9

Friction Loss = 1.11 ft/100ft of pipe

3. Determine total pipe length from pump discharge to soil treatment discharge point. Estimate by adding 25 percent to pipe length for fitting loss. Total pipe length times 1.25 = equivalent pipe length

30 feet x 1.25 = 37.5 feet

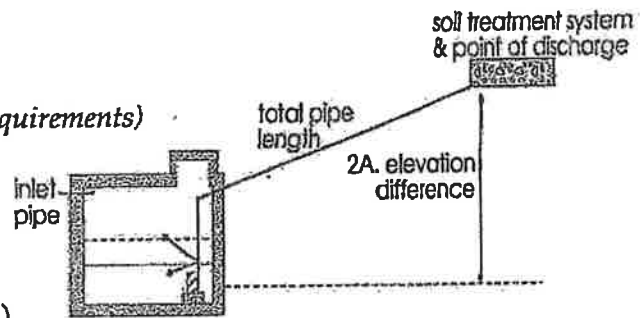
4. Calculate total friction loss by multiplying friction loss (C2) in ft/100 ft by the equivalent pipe length (C3) and divide by 100.

= 37.5 ft/100ft x 1.11 ÷ 100 = .4 ft

D. Total head required is the sum of elevation difference (A), special head requirements (B), and total friction loss (C4)

7 ft + 5 ft + .4 ft =

Total head: 12.4 feet



Special Head Requirements	
Gravity Distribution	0 ft
Pressure Distribution	5 ft

flow rate gpm	E-9: Friction Loss in Plastic Pipe Per 100 feet		
	nominal pipe diameter		
	1.5"	2"	3"
20	2.47	0.73	0.11
25	3.73	1.11	0.16
30	5.23	1.55	0.23
35	6.96	2.06	0.30
40	8.91	2.64	0.39
45	11.07	3.28	0.48
50	13.46	3.99	0.58
55		4.76	0.70
60		5.60	0.82
65		6.48	0.95
70		7.44	1.09

3. Pump selection

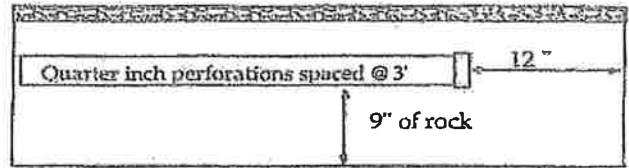
A pump must be selected to deliver at least 22.2 gpm (1A or B) with at least 12.4 feet of total head (2D)

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Barry E. Jahl (signature) 42006 (license #) 4/17/2024 (date)

PRESSURE DISTRIBUTION SYSTEM

Geotextile fabric



Perf Sizing 3/16" - 1/4"
Perf Spacing 1.5' - 5'

E-4: Maximum allowable number of 1/4-inch perforations per lateral to guarantee <10% discharge variation

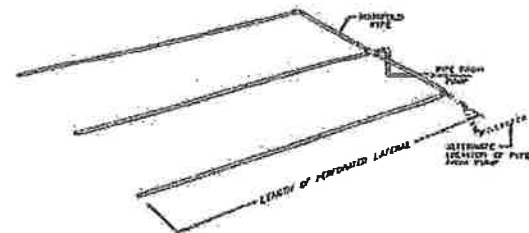
perforation spacing (feet)	1 inch	1.25 inch	1.5 inch	2.0 inch
2.5	8	14	18	28
3.0	8	13	17	26
3.3	7	12	16	25
4.0	7	11	15	23
5.0	6	10	14	22

E-6: Perforation Discharge in gpm

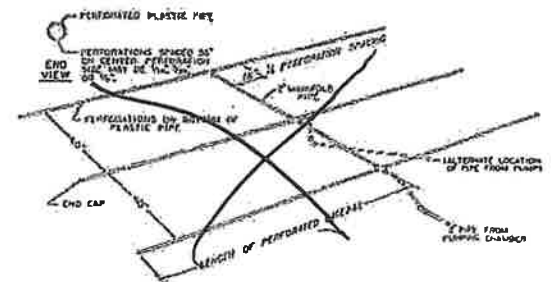
head (feet)	perforation diameter (Inches)			
	1/8	3/16	7/32	1/4
1.0 ^a	0.18	0.42	0.56	0.74
2.0 ^b	0.26	0.59	0.80	1.04
5.0	0.41	0.94	1.26	1.65

^a Use 1.0 foot for single-family homes.
^b Use 2.0 feet for anything else.

MANIFOLD LOCATED AT END OF PRESSURE DISTRIBUTION SYSTEM



LAYOUT OF PERFORATED PIPE LATERALS FOR PRESSURE DISTRIBUTION IN MOUND



1. Select number of perforated laterals 3

2. Select perforation spacing = 2.5 ft

3. Since perforations should not be placed closer than 1 foot to the edge of the rock layer (see diagram), subtract 2 feet from the rock layer length.

$$\frac{25}{\text{Rock layer length}} - 2 \text{ ft} = 23 \text{ ft}$$

4. Determine the number of spaces between perforations. Divide the length (3) by perforation spacing (2) and round down to nearest whole number.

$$\text{Perforation spacing} = \frac{23 \text{ ft}}{2.5 \text{ ft}} = 9 \text{ spaces}$$

5. Number of perforations is equal to one plus the number of perforation spaces(4). Check figure E-4 to assure the number of perforations per lateral guarantees <10% discharge variation.

$$9 \text{ spaces} + 1 = 10 \text{ perforations/lateral}$$

6. A. Total number of perforations = perforations per lateral (5) times number of laterals (1)

$$10 \text{ perfs/lat} \times 3 \text{ lat} = 30 \text{ perforations}$$

B. Calculate the square footage per perforation.

Should be 6-10 sqft/perf. Does not apply to at-grades.

Rock bed area = rock width (ft) x rock length (ft)

$$10 \text{ ft} \times 25 \text{ ft} = 250 \text{ sqft}$$

Square foot per perforation = Rock bed area ÷ number of perfs (6)

$$\frac{250 \text{ sqft}}{30 \text{ perfs}} = 8.3 \text{ sqft/perf}$$

7. Determine required flow rate by multiplying the total number of perforations (6A) by flow per perforation (see figure E-6)

$$30 \text{ perfs} \times 0.74 \text{ gpm/perfs} = 22.2 \text{ gpm}$$

8. If laterals are connected to header pipe as shown on upper example, to select minimum required lateral diameter; enter figure E-4 with perforation spacing (2) and number of perforations per lateral (5) Select minimum diameter for perforated lateral = 1.8 inches.

9. If perforated lateral system is attached to manifold pipe near the center, lower diagram, perforated lateral length (3) and number of perforations per lateral (5) will be approximately one half of that in step 8. Using these values, select minimum diameter for perforated lateral = _____ inches.

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Bruce E. Galt

(signature)

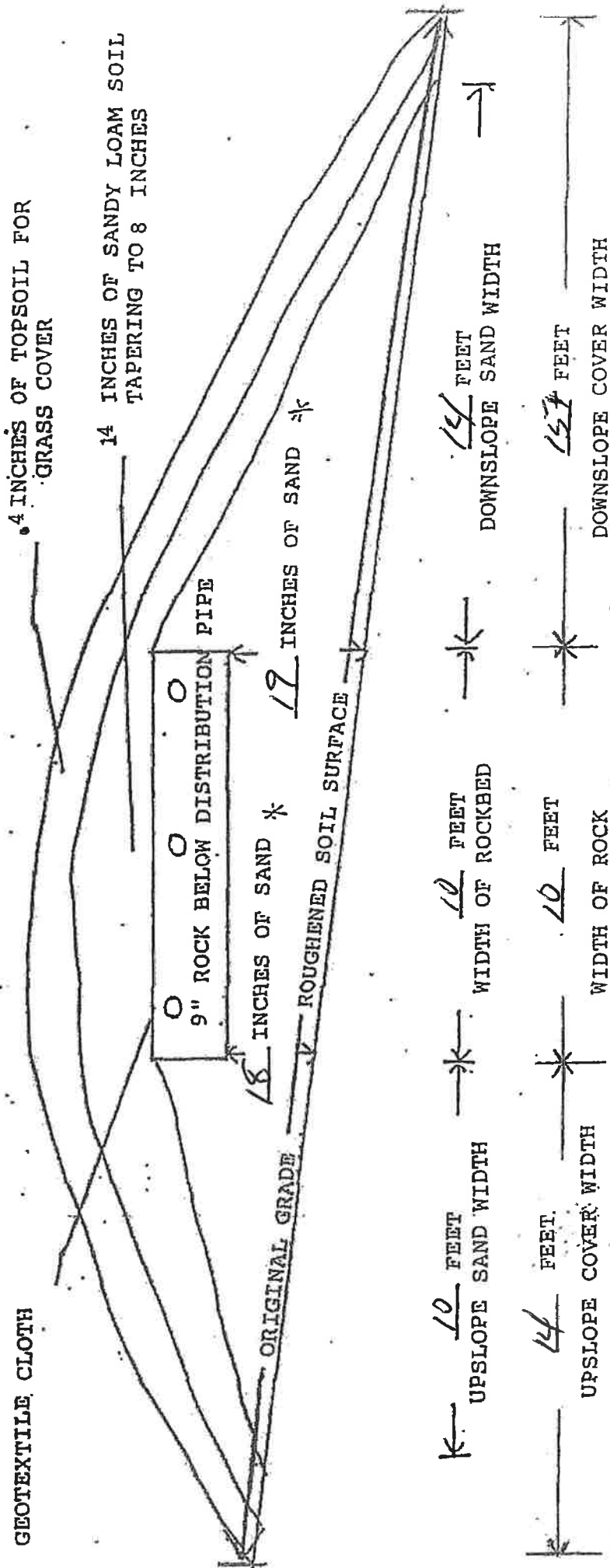
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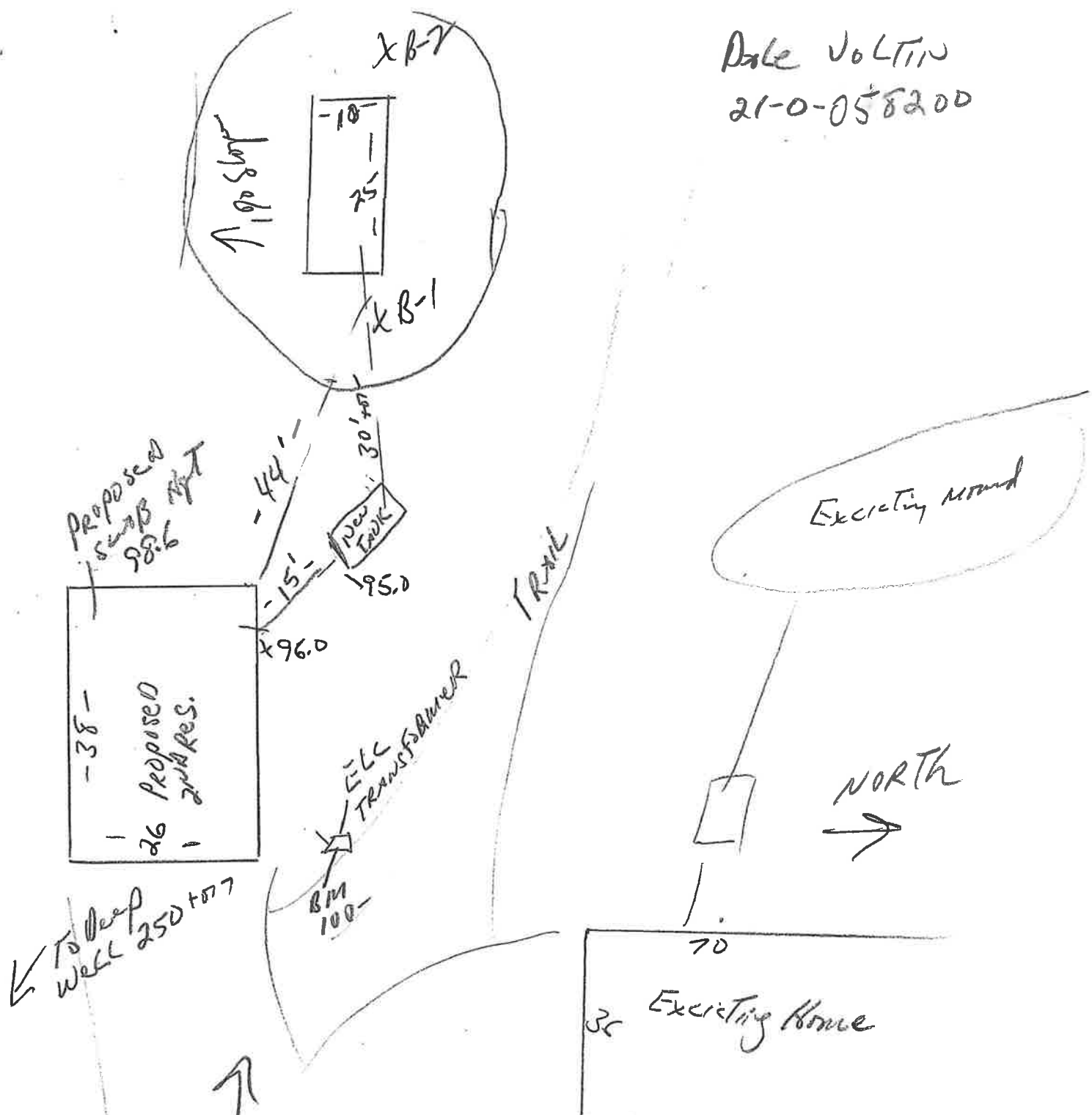
4/17/2024 (date)

MOUND CROSS-SECTION

12 PERCENT SLOPE OF ORIGINAL SOIL
10 FT. x 25 FT. SIZE OF ROCKBED 34 FT. x 45 FT. SIZE OF SANDBASE



Date VOLTIN
21-0-058200



TO DEEP WELL 250 FT

TO ALL PROPERTY LINES

- 100 BENCHMARK TOP OF TRANSFORMER
- 98.6 PROPOSED SLAB HGT
- 96.0 PROPOSED LINE TO HOME
- 95.0 TANK INLET
- 92.0 PUMP HGT
- 98.1 SAND HGT
- 99.0 DISCHARGE HGT
- 7.0 LIFT.

Dave Dahl
L2006 4/17/24

Dale VOLTIN

210-058200

SOILS CHARTS FOR BOTH PROPOSED AND ALTERNATE SITES

1 (PROPOSED) SOILS DATA

b-2

DEPTH (INCHES)	TEXTURE	MUNSELL COLOR
0-4	T.S Loam Roots No Rocks Friables	10YR 3/2
4-18	Fine Sand Loam Friable No Rocks Roots	10YR 4/3
18+	Gravel Rocky	
* Mostly wet		7.5YR 4/4

2 (PROPOSED) SOILS DATA

b-1

DEPTH (INCHES)	TEXTURE	MUNSELL COLOR
0-5	T.S Roots FRIBLE No Rocks Loam	10YR 2/2
5-18	FINE SAND Loam Roots FRIBLE NO ROCKS	10YR 3/3
18+	Gravel	7.5YR 4/4
* Wet at this time		

1 (ALTERNATE) SOILS DATA

DEPTH (INCHES)	TEXTURE	MUNSELL COLOR

2 (ALTERNATE) SOILS DATA

DEPTH (INCHES)	TEXTURE	MUNSELL COLOR

* Note: Early Season Ground still wet.
 Didnt see Redox AT Gravel Layer
 ADDITIONAL SOIL BORINGS MAY BE REQUIRED



Search

Map Unit Legend

Aitkin County, Minnesota (MN001)

Aitkin County, Minnesota (MN001)

Map Unit Symbol	Map Unit Name	Acres In AOI	Percent of AOI
C4A	Cebana-Giese, frequently ponded-Ronneby complex, 0 to 3 percent slopes, stony	3.3	11.7%
C9B	Mora-Ronneby complex, 1 to 4 percent slopes, stony	3.9	13.7%
C28A	Cathro-Twig, stony complex, 0 to 1 percent slopes, frequently ponded	8.6	30.2%
C72D	Milaca-Millward complex, 2 to 20 percent slopes, stony	0.6	2.1%
C73C	Milaca loam, 1 to 7 percent slopes, stony	9.7	34.1%

Soil Map

Scale (not to scale)



Warning: Soil Map may not be valid at this scale.

You have zoomed in beyond the scale at which the soil map for this area is intended to be used. Maps at particular scale. The soil surveys that comprise your AOI were mapped at 1:20,000. The design of maps shown in the resulting soil map are dependent on that map scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of map placement. The maps do not show the small areas of contrasting soils that could have been shown at