OSTP Field Evaluation Form

Contact Information Property Owner/Cl	ient p				1
١		Maples Proj	ect ID: Test 1		>
Date 10/3/2021	2042 VIKING BLV	D. NE Codon Miles			-1
		Conditions Conditions	1 30	Client Phone Number: 763-234-318	v 03
2. Utility and Structure Infor	mation		1 Tal		9
Utility Locations Identified				Cloudy	
	Gopher State One C	ali#			
Property Lines		1	Any Private Utilities		
	Determined and App	roved by Client			
	Determined but not A	pproved		Client's	
	Approximate			Client's Approval (initial)	
Ocata	Property Lines Surveye	ad			
Locate and Verify (see Site Evalu	ation man)				
	Existing Buildings				
		Improvements	Easements		
. Site Information			-adding is	Setbacks	
Percent Slope					
Landscape Position	4		CI.		
	Foot		Slope Direction		
Vegetation type(s)			Slope Shape Co	oncave West	
Evidence of cut, fill, comp	acted or disturbed ar	eas Yes	Wooded		
Discuss the flooding or	run-on potential of	11.	No erted around mound area.		
	proceeded of S	ite All water to be dive	erted around mound area		
Identify bond			area.		
Posed soil treatment	imarks and elevations	(Site Evaluation Map)	Ronch		
posed soil treatment area adequ	ately protected	Yes	. so, existing	garage floor	
General Soils Information			No		
ginal soils					
o of alt.	Yes	No			
e of observation	Soil Probe	Soil Boring	7		
nber of soil observations	2	7	Soil Pit		
observations were conducted in i	- L	_			
il observation was made within a	the proposed system (ocation	Yes No		
il observation was made within the	ne most limiting area	of the proposed system	Yes No		
and a completed and a	attached	. V			1
olation tests performed, forms co	ompleted and attache	d Yes No			1
					1
hase I. Reporting Information		The state of the s			
Depth to standing water		inches			
Flood elevation	215	1	Antici	pated construction issues	
Depth to bedrock	2132	feet			1
th to periodically saturated soil		inches	ZZZZZSKI SKOTO SKOTO		1
	24	inches			1
Maximum depth of system	Mound	inches			1
Elevation at system bottom	104	feet	Difference		
Percolation rate		min/inch	Soil Summer of the Control of the Co	een soil survey and field evaluation	ĺ
Loading rate	0.79		Soil Survey states- C72 D, I		NAME OF TAXABLE PARTY.
		gpd/ft ²	Soils on site are a sandy lo	am soil with large rocks at 25"	
Contour loading rate	12	gpd/ft			
Contour loading rate					1
Contour loading rate evaluation issues / comments					1

(Signature)

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OF MINNESOTA OSTP Soil Observation Log Project ID: Test 1

The same of the sa				-			riojectio.	i est i	V 03.19.15	
С	lient/ Address	:		Bruce Ma	ples	Legal Des	cription/ GPS:	S110' Of N8		of n870' NE NW, Sec17
Soil parent	material(s): (Check all	that apply	/) <u> </u>	Outwash Lacustrin	e Loess	Till [] Allu	-		nic Matter
Landscape I	Position: (ched	ck one)	Summ	it Sho	oulder Back/Side Sk	ppe Foot Slope	Toe Slop	oe Slope s hape		convex
Vegetation	7	wooded		So	oil survey map units	C72D	Slope%	4.0	Elevation:	102
Weather Co	nditions/Time	of Day:			Cloudy 10:0	00 AM		Date	1	0/03/21
Observation	on #/Location:		Soil Borir	ng #1, Nor	th west end of syste	em area	Obse	ervation Type:		Auger
Depth (in)	Texture	Rock Frag. %	Matrix	Color(s)	Mottle Color(s)	Redox Kind(s)	Indicator(s)		Structure	
		1145.70					```	Shape	Grade	Consistence
6	Loam	<35%	10YR	2/2				Single grain	Weak	Friable
19	Loamy Sand	<35%	10YR	4/4				Single grain	Weak	Friable
20	Loamy Sand	35-50%	10YR	4/4	7.5YR 4/3	Concentrations, depletions, gleyed	S1	Single grain	Structureless	Friable
Comments										
Trea	fy that I have of the second o	lund	this work	in accorda	ance with all applica	able ordinances, r	ules and laws	663		10/3/21
715	mispector		NAMES AND DESCRIPTION OF THE PARTY OF THE PA	-	(Signáture)	CONTROL CONTRO		(License #)	***	(Date)

University of Minnesota

OSTP Soil Observation Log

Project ID: Test 1

v 03.19.15



Client/ Address:			В	ruce Map	les	Legal Desc	ription/ GPS:	S110' Of N87	'0' Lot 1& s100',o	f n870' NE NW, Sec17
Soil parent r	material(s): (C	heck all t	hat apply)		Outwash Lacustrine	e Loess .	Till Alluv	ium Bedr	ock Organi	ic Matter
Landscape P	osition: (chec	k one)	Summit	: Shou	ulder Back/Side Side	ppe Foot Slope	Toe Slope	e Slope shape	convex	
Vegetation		wooded		Soi	il survey map units	C72D	Slope%	4.0	Elevation:	102
Weather Cor	nditions/Time	of Day:			Cloudy 10:0	Cloudy 10:00 AM Date 10/03/21				
Observatio	n #/Location:		Soil Borin	ng #2 Sout	th west end of syste	em area	Obse	rvation Type:		Auger
Depth (in)	Texture	Rock	Matrix (Color(s)	Mottle Color(s)	Redox Kind(s)	Indicator(s)		Structure	
		Frag. %						Shape	Grade	Consistence
8	Loam	<35%	10YR	2/2				Single grain	Weak	Friable
20	Loamy Sand	<35%	10YR	4/4				Single grain	Weak	Friable
21	Loamy Sand	35-50%	10YR	4/4	7.5YR 4/3	Concentrations, depletions, gleyed	S1	Single grain	Structureless	Friable
1										
	p - gr									
			PORTE TO THE STATE OF THE STATE							
Comments										
Grega	Weste	Lunc	1 9	n accord	dance with all applic	pable ordinances,	rules and laws	663		10/3/21
(mesi	(Designer/Inspector) (Signature) (License #) (Date)								/ '(Date)'	

OSTP Mound Design Worksheet

Minnesota Pollution

Control Agency

University of Minnesota



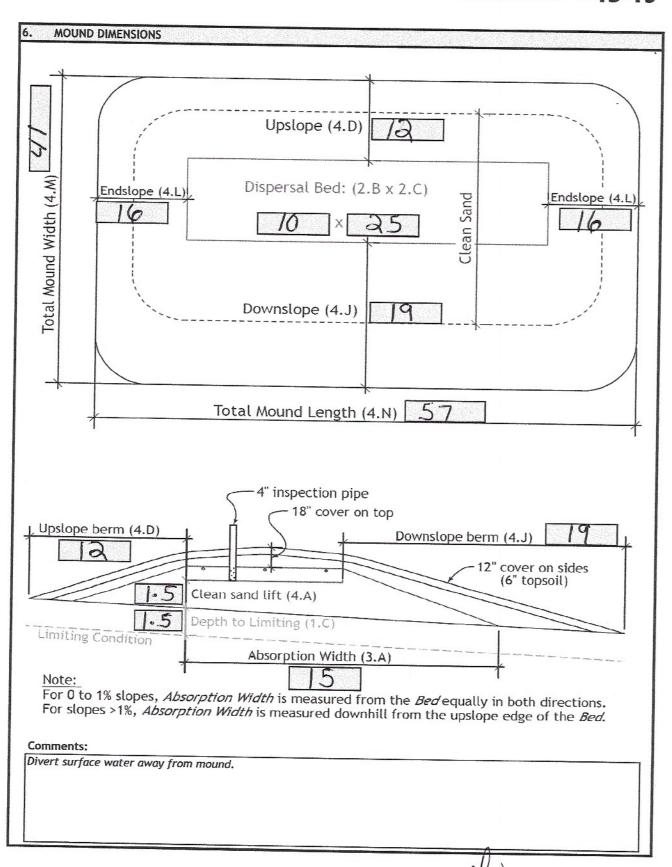
1. SYSTEM SIZING:								
A. Design Flow (Flow & Soil - 1.A) :	300	GPD			Table I			
B. Soil Loading Rate (Flow & Soil-3.C):	70	GPD/ft ²	-	MOUN	D CONTOUR LOADING RATE	S: Contaur		
C. Depth to Limiting Condition:	- 7	ft	Measured Perc Rate	OR	Texture - derived mound absorption ratio	Loading Rate:		
D. Percent Land Slope:	11	%	≤ 60mp1		1.0, 1.3, 2.0, 2.4 2.6	±12		
E. Design Media Loading Rate:	1-20	GPD/ft ²	61-120 mpi	OR	5.0	£12		
F. Mound Absorption Ratio (1.E÷1.B):	1.5		2 (20 mpi*			26"		
G. Design Contour Loading Rate:	12	GPD/ft	*Systems w	ith th	ese values are not Type I s	systems.		
(From Table I - same as Linear Loadi	ng Rate)				Rate is a recommended va	5		
2. DISPERSAL MEDIA SIZING								
A. Calculate Required Dispersal Bed Are	ea: Design Flow	/ (1 Δ) ± Dos	ian Media I	oadir	na Rate (1 F) = ft ²			
Januaria Rayan tu Dispersur Deu Art					f			
If a larger dispersal media area is desired, enter size: $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								
B. Calculate Dispersal Bed Width: Contour Loading Rate (1.G) ÷ Design Media Loading Rate (1.E) = Bed Width								
	$ft \div gpd/ft^2 = ft$							
C. Calculate Dispersal Bed Length: Disp	persal Bed Area	(2.A) ÷ Bed	Width (2.E	B = B	ed Length			
	250	ft ² ÷	O ft	= [25 ft			
D. Select Dispersal Media:	ock							
	her Approve	d Media (D	escribe):					
3. ABSORPTION AREA SIZING								
Note: Mound setbacks are measured	from the Absor	rntion Area				-		
		•	5-41-44	-				
A. Calculate Absorption Width: Bed Wid	1	ft X	on Katio (1	.r) = . =	Absorption Width			
B. For slopes from 0 to 1%, the Absorpt	ion Width is me	easured from	the bod or	بالديد	in both directions			
Calculate Absorption Width Beyond to						and Pad		
I		ft -	(3.A) - Bea	. T	n (2.6) ÷ 2 = wiath bey			
		L		L		ft		
C. For slopes >1%, the Absorption Width								
Calculate Downslope Absorption Wid	th: Absorption	Width (3.A)	- Bed Widt	h (2.	B) = ft			
	15	ft -	O ft	=	5 ft			
Comments:	100,000,000,000,000,000,000,000							
Slope, CLR Choice, Material issues								
1								

13-18 ■ SECTION 13: Forms and Reference

4. MOUND SIZING
A. Calculate Clean Sand Lift: 3 feet minus Depth to Limiting Condition (1.C) = Clean Sand Lift (1 ft minimum)
3.0 ft - $1 \circ 5$ ft = $1 \circ 5$ ft
B. Calculate Upslope Height: Clean Sand Lift (4.A) + media depth (1 ft.) + cover (1 ft.) = Upslope Height
[1.5] # + ft + ft = 3.5 ft
D-34: Slope Multiplier Table Land Slope % 0 1 2 3 0 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25
Upslope 3:1 3.00 2.91 2.83 2.75 2.68 2.61 2.54 2.48 2.42 2.36 2.31 2.26 2.71 2.13 1.4 15 16 17 18 19 20 21 22 23 24 25 Berm Ratio 4:1 4.00 3.85 3.70 3.57 3.45 3.33 3.23 3.12 3.03 2.94 2.86 2.78 2.70 2.62 2.55 2.48 2.41 2.35 2.29 2.23 2.18 2.13 2.08 2.03 1.98 1.93
Land Slope % 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 Downslope 3:1 3.00 3.09 3.19 3.30 3.41 3.53 3.66 3.80 3.95 4.11 4.29 4.48 4.69 4.95 5.74 5.55 5.88 6.74 6.63 7.03 7.07 7.03 8.00 0.01
Downstope 3:1 3.00 3.09 3.19 3.30 3.41 3.53 3.66 3.80 3.95 4.11 4.29 4.48 4.69 4.95 5.24 5.55 5.88 6.24 6.63 7.04 7.47 7.93 8.42 8.93 9.46 10.02 8erm Ratio 4:1 4.00 4.17 4.35 4.54 4.76 5.00 5.26 5.56 5.88 6.25 6.67 7.14 7.69 8.29 8.92 9.57 10.24 10.94 11.67 12.42 13.19 13.99 14.82 15.67 16.54 17.44
C. Select Upslope Berm Multiplier (based on land slope): (figure D-34)
D. Calculate Upslope Berm Width: Multiplier (4.C) X Upslope Mound Height (4.B) = Upslope Berm Width
[3.45] ft x $[3.5]$ ft = $[2.1]$ ft
E. Calculate Drop in Elevation Under Bed: Bed Width (2.B) X Land Slope (1.D) ÷ 100 = Drop (ft)
ft X 4/ % ÷ 100 = 94/ ft
F. Calculate Downslope Mound Height: Upslope Height (4.B) + Drop in Elevation (4.E) = Downslope Height
3.5 ft + 4 ft = 3.9 ft
G. Select Downslope Berm Multiplier (based on land slope): 4-76 (figure D-34)
H. Calculate Downslope Berm Width: Multiplier (4.G) X Downslope Height (4.F) = Downslope Berm Width
4.76 × 3.9 ft = 18.6 ft
I. Calculate Minimum Berm to Cover Absorption Area: Downslope Absorption Width (3.B or 3.C) + 4 ft. = ft
$\int_{0}^{\infty} \int_{0}^{\infty} \int_{0$
J. Design Downslope Berm = greater of 4H and 4I: 18.6 ft
K. Select Endslope Berm Multiplier: (usually 3.0 or 4.0)
L. Calculate Endslope Berm (4.K) X Downslope Mound Height (4.F) = Endslope Berm Width
4 ft x 3-9 ft = 15.6 ft
M. Calculate Mound Width: Upslope Berm Width (4.D) + Bed Width (2.B) + Downslope Berm Width (4.J) = ft
10-1 ft + 10 ft + 18.6 ft = 4/1.7 ft
N. Calculate Mound Length: Endslope Berm Width (4.L) + Bed Length (2.C) + Endslope Berm Width (4.L) = ft
15.6 ft + 25 ft + 15.6 ft = 56.2 ft
ORGANIC LOADING: (Optional)
A. Organic Loading = Design Flow X Estimated BOD in mg/L in the effluent X 8.35 ÷ 1,000,000
gpd X mg/L X 8.35 ÷ 1,000,000 = lbs BOD/day
B. Calculate System Organic Loading: lbs. BOD (5.A) ÷ Bed Area (2.A) = lbs/day/ft ²
$lbs/day \div $
C. Recommended Organic Loading Rate: lbs/day/ft ²



SECTION 13: Forms and Reference ■ 13-19



13-20 ■ SECTION 13: Forms and Reference

7.	nio-tes	APPROXIMATE MOUND MATERIAL CALCULATIONS:
1	۹.	Calculate Bed (rock) Volume: Bed Length (2.C) X Bed Width (2.B) X Depth = Volume (ft ³)
		$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
		Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards:
		$250 \text{ ft}^3 \div 27 = 9 \cdot 26 \text{ yd}^3$
		Add 20% for constructability: $9.26 \text{ yd}^3 \text{ X} 1.2 = //_{P}/\text{yd}^3$
E	3.	Calculate Clean Sand Volume:
		Upslope Volume: $((Upslope\ Mound\ Height-1) \times 3 \times Bed\ Length) \div 2 = cubic\ feet$
		$((3.5 \text{ ft - 1}) \text{ x} 3 \text{ ft x} 25) \div 2 = 93.75 \text{ ft}^3$
		Downslope Volume: ((Downslope Height - 1) x Downslope Absorption Width x Media Length) ÷ 2 = cubic feet
		(($3-9$ ft -1) x 5 ft x 25) ÷ 2 = 362.5 ft ³
		Endslope Volume: (Downslope Mound Height - 1) x 3 x Media Width = cubic feet
		$(3.9 \text{ ft} - 1) \times 3 \text{ ft} \times 10 \text{ ft} = 87 \text{ ft}^3$
		Volume Under Rockbed: Average Sand Depth x Media Width x Media Length = cubic feet
		1-7 ft x 10 ft x 25 ft = 425 ft ³
		Total Clean Sand Volume : Upslope Volume + Downslope Volume + Endslope Volume + Volume Under Media
		93-75 ft ³ + $362-5$ ft ³ + 87 ft ³ + 425 ft ³ = $968-36$ ft ³
		Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: $968 - 35 \text{ ft}^3 \div 27 = 35 - 86 \text{ yd}^3$
		Add 20% for constructability: $35-86 \text{ yd}^3 \text{ x } 1.2 = 43-03 \text{ yd}^3$
(Calculate Sandy Berm Volume:
		Total Berm Volume (approx): ((Avg. Mound Height5 ft topsoil) x Mound Width x Mound Length) ÷ 2 = cu. ft.
		$(57) \div 2 = 3,990 \text{ ft}^3$
		Total Mound Volume - Clean Sand volume -Rock Volume = cubic feet
		968 5 ft3 - 250 ft3 - 3,990 ft3 = 277/05 ft3
		Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: $2771.5 \text{ ft}^3 \div 27 = 100.65 \text{ yd}^3$
		Add 20% for constructability: $yd^3 \times 1.2 = \sqrt{0.3.85} yd^3$
D).	Calculate Topsoil Material Volume: Total Mound Width X Total Mound Length X .5 ft
		40 ft x 57 ft x 0.5 ft = $1,140$ ft ³
		Divide ft ³ by 27 ft ³ /yd ³ to calculate cubic yards: $1140 ext{ ft}^3 \div 27 = 42 \cdot 2 ext{ yd}^3$
		Add 20% for constructability: $\frac{4}{3} \cdot 3 \text{yd}^3 \times 1.2 = 50 \cdot 66 \text{yd}^3$
	es rece	

i nereby certify that I have completed this W	ork in accordance with all app	plicable ordinances,	rules and laws.
Grea Westerlund	collection	663	10/4/21
(Designer)	(Signature)	(License #)	(Date)

13-24 ■ SECTION 13: Forms and Reference

Minnesota Pollution

OSTP Pressure Distribution Design Worksheet

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Cor	ntrol Agency	Coign V	VOI KSITEE		OF MINNES	OIA	517
1.	Select Number of Perforated Laterals in (2 feet is minimum and 3 feet is maximu. Select Perforation Spacing:		3	Sealth Sealth Sealth Sealth Seal		linmum Silini of rock	
3.	Select Perforation Diameter Size			nch	Perforation sizing 1/2 to Perforation spacing 2/2 to		
4.	Length of Laterals = Media Bed Length -	distance from 6		feet depending on ma nen 1 foot from edge)	nifold location as	perfs can not	be
	25 ft - 2 ft = 3	3 ft					
5.	Determine the <i>Number of Perforation Sp.</i> round down to the nearest whole number		ne Length of Late	rals (Line 4) by the F	Perforation Spacin	g (Line 2) and	Í
	Number of Perforation Spaces =	23 ft	÷ 3	ft =	7 Space	es	
6.	Number of Perforations per Lateral is eq	ual to 1.0 plus	the Number of P	erforation Spaces (Lin	ne 5).		
	Perforations Per Lateral = 7	Spaces	+ 1	= 8 p	erfs. Per Lateral		
	Check Table I to verifty the number of potential the a center manifold is used.	erforations per	lateral guarante	es less than a 10% disc	charge variation.	The value is a	louble if
7.	Total Number of Perforations equals the Perforated Laterals (Line 1).	Number of Per	forations per Lat	eral (Line 6) multiplie	ed by the <i>Number</i>	of	
	Perf. Per Lateral X	3	Number of Perf	. Laterals =	24 Tota	l Number of Po	erf.
8.	Calculate the Square Feet per Perforation	n. Recommend	led value is 4-10 j	ft ² per perforation.		Table III	
	Does not apply to At-Grades				The state of the s	ion Discharge (GPM)	
	Bed Area = Bed Width (ft) X Bed Length	(ft)				Perforation Diamet	
	10 ft x 25	ft =	250 f	.2	Head (ft) 1/6	0.41 0.56	0.74
	Square Foot per Perforation = Bed Area	divided by the	Total Number of	Perforations (Line 7).	2.0° 0.26 5.0° 0.41	0.59 0.80 0.93 1.26	1.04
	250 ft2 + 24	perforations	1.00	ft ² /perforations	a: Use 1.0 for dwellin holes. b: Use 2.0 for dwellin	ngs using 1/8 mch bo	oles: or, for
9.	Select Minimum Average Head:	ft		-	other establishments holes. c: Use 5.0 for other e	establishments using	
10.	Select Perforation Discharge (GPM) based	d on Table III:	07	GPM per Perfora	perforations and med ation	lia filters	-
11.	Determine required Flow Rate by multiple	ying the Total	Number of Perfo	rations (Line 7) by the	Perforation Disc	harge (Line 10)).
	QΥ Perforations X Θ	74 GPM p	er Perforation	= 17.76	GPM		
12.	Select Type of Manifold Connection (End	or Center):	€ End □] Center			

OSTP Pressure Distribution Design Worksheet

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> Table II Volume of Liquid in

> > **Pipe**

Liquid

Per Foot

(Gallons)

0.045

0.078 0.110

0.170

0.380

0.661

Pipe

Diameter

(inches)

1.25

1.5 2

3



	max.	mun mun	per or heu	rorations P	er Latera	l to Guarantee < 10% Disc	charge Va	nothern				
, Inch Perforations							7/32	nch Perfor	ations			
Perforation Spacing (Feet)		Fipe [hameter ()	nches)		Perforation Spacing Pipe Diameter (In				nches)	(ches)	
	1	1.5	1/4	2	3	(Feet)	1	134	1%	T] 3	
	10	13	18	30	50	į.	11	16	2	34	€8	
2 t	8	12	16	18	54	214	10	3-4	20	32	64	
3	8	12	16	25	52	3	9	14	19	30	60	
	3 16 Inch	Perforatio	ns				181	nct Perfor	ations		***************************************	
Perforation Spacing (Feet)		Fipe D	iameter (I	nches)		Perforation Spacing		Pipe :	hameter il	nches		
	1	174	1+1	2	3	(Feet)	1	154	115	1	3	
2	12	13	26	46	37	2	21	33	44	74	149	
2.5	12	17	24	40	30	2%	20	30	4	69	135	
3	12	15	22	57	75	1 3	20	25	38	64	128	

14. Select Lateral Diameter based on Table I:



in

15. Volume of Liquid Per Foot of Distribution Piping:

ì		-	
	-/		Gallons/fi

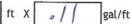
- 16. Volume of Distribution Piping =
 - = [Number of Perforated Laterals (Line 1) X Length of Laterals (Line 4) X (Volume of Liquid Per Foot of Distribution Piping (Line 15)]



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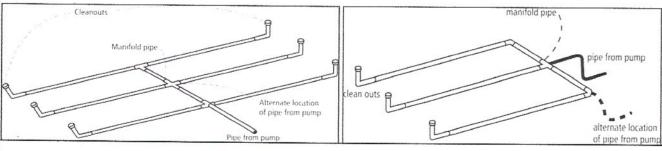




		_
=	7.59	Gallons

17. Minimum Dose = Volume of Distribution Piping (Line 17) X 5





I hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws.

(Designer)

(Signature)

13-30 ■ SECTION 13: Forms and Reference

		O215 Samb Selec	tion D	esign	Ī	INIVE	RSITY			
Minnesota Control	Pollution Agency	Workshe	eet				NESOT	A 📄	2-1-	
1. PUMP C	APACITY									
A. Pumpi	ng to Gravity or Pressure D	istribution: O Gravity	Pressure							
1. If p	oumping to gravity enter the	gallon per minute of the pump:		GPM						
		oump for the treatment system or t	he collection	system:						
0	Treatment System O Collection	on System								
		atment system, what part or type o	of system:							
<u>S</u>	Soil Treatment	□Media Filter □Other								
	umping to a pressurized dist of Pressure Distribution or Line 10	tribution system: O of Non-Level or enter if Collection System	1/8	GPM						
2. HEAD R	EQUIREMENTS									
	ion Difference	ft ft		-		ing length		& point of	discharge	
system		subsurface sewage treatment ystem is a Collection System, Step 10.	inlet pipe	To be a second s	Steph	South has length Elevation difference				
4. Distrib	ution Head Loss:	ft								
5. Addition	onal Head Loss:	ft (due to special equip	oment, etc.)							
	Distributio	n Head Loss		Friction	Loss i			per 10	0 ft	
Gravity	Distribution = Oft	ALL			Nomin	(C=13		ter		
1 1	e Distribution based on On Pressure Distribution	on Minimum Average Head on Worksheet:		Flow Rate (GPM)	1	11/4	11/2	2	3	
Minis	num Average Head	Distribution Head Los	s	10	9.11	3.08	1.27	0.31		
	1ft	5ft	_	12	12.77	4.31	1.78	0.44		
l 	2ft 5ft	6ft 10ft	_	14	16.99	5.74	2.36	0.58		
	310	1016		16		7.35	3.03	0.75	0.10	
6. A. Sup	ply Pipe Diameter:	2 in		(18)		9.14	3.76		0 ft 3 0.10 0.13 0.44 0.57 0.70 0.86 1.02 1.20 1.39	
				20		11.11	4.58	And in case of the last of the		
B. Sup	ply Pipe Length:	185 ft		25		16.79				
7 Pered	an Faistina I ann in Blantin S	Dina and 400ft from Table Is		30		10.75	9.69			
7. based	on Friction Loss in Plastic F	Pipe per 100ft from Table I:		35			12.90			
Frictio	n Loss =	ft per 100ft of pipe		40			16.52	2 3 0.31 0.44 0.58 0.75 0.10 0.93 0.13 1.13 0.16 1.71 0.24 2.39 0.33 3.18 0.44 4.07 0.57 5.07 0.70 6.16 0.86 7.35 1.02 8.63 1.20 10.01 1.39 11.48 1.60		
111000		J reper roote or pipe		45			10.52		Der 100 ft er 2 3 0.31 0.44 0.58 0.75 0.10 0.93 0.13 1.13 0.16 1.71 0.24 2.39 0.33 3.18 0.44 4.07 0.57 5.07 0.70 6.16 0.86 7.35 1.02 8.63 1.20 10.01 1.39 11.48 1.60	
8. Deterr	nine Equivalent Pipe Length	from pump discharge to soil dispe	rsal	50						
area d	ischarge point. Estimate by	adding 25% to supply pipe length f	or	55						
fitting	loss. Supply Pipe Length (5	i.B) X 1.25 = Equivalent Pipe Lengt	h							
110	75	2012		60						
	ft X 1.2	25 = 33 est ft		65			~ ~ ~			
o Calcul	ata Cunniu Friction Loss ha	multiplying Friction Loss Per 100ft	(line 4) by	70	Dine Ler	ath () in	 2 7) and			
	Friction Loss =	23/25	(Line o) by (are Equivalent	i ipe Leli	sen (cili	c / j and	arride by	.00.	

• 93 ft per 100ft

OSTP Pump Selection Design Worksheet

University of Minnesota

Minnesota Pollution Control Agency

Section 10 is for Collection Systems ONLY and does NOT need to be completed for individual subscript ce sewage treatment systems. Quantity X Equivalent Length Factor = Equivalent Length Fitting Type Quantity	D. Equivalent length of pipe fittings.					Equivalent Lengt	h Factors	(ft.) for P	VC Pipe		
Quantity X Equivalent Length Factor = Equivalent Length Fitting Type											
Quantity X Equivalent Length Factor = Equivalent Length Fitting Type								Fitting Type			¥T
Fitting Type Quantity Equivalent Length (t) Equivalent Length (t) Code Valve								Gate Valve			2.04
Fitting Type Quantity Length Factor Length (ft) Gate Valve X	Qualitity x Equivalent	Length Factor =	Equiva	tent Length				90 Deg Elbow	4.03	5.17	7.67
Gale Valve			i		I		1	45 Deg Elbow	2.15	2.76	4.09
Gate Valve	Fitting Type	Quantity						Tee - Flow Thru	2.68		5.11
Gate Valve X = 00 Deg Elbow X = 00 Tes Elbow				Length Factor		Length (ft)		Tee - Branch Flow	8.05	10.30	15.30
Some Various	C-4- 1/-1-		х		=						25.50
## SD beg Elbow	Gate valve				-		-				38.40
45 Deg Elbow Tee - Flow Thru Tee - Branch Flow X = NOTE: Equivalent length values for PVC pipe fittings are based on calculations using the Hazen- Williams Equation. See Advanced Designs for SSTS Angle Valve X = Globe Valve X = Hazen-Williams Equivalent length factors. Verify other equivalent length factors with pipe material manufacturer. NoTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + If t = If t Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + If t = If t Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + If t = If t Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + If t = If t Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t + If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t Total Pipe Length (10.8) If t = If t = If t Total Pipe Length (10.8) If t = If t = If t Total Pipe Length (10.8) If t = If t = If t = If t = If t Total Pipe Length (10.8) If t = If	90 Deg Elbow		Х		=				45.60		86.90
To the Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) ft + Hazen-Williams Fountion loss due to pipe fittings and supply pipe (h _t): (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8) (10.5 + Pipe Diameter AST) X (Flow Rate + Constant) S X Total Pipe Length (10.8)	45 Deg Elbow		Х		=			butterny valve		7.73	11.50
Swing Check Valve $\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Tee - Flow Thru		Х		=						
Swing Leck Valve Angle Valve A	Tee - Branch Flow		Х		=		N	OTE: Equivalent length	values for I	PVC pipe	
Angle Valve X $=$ for equation. Other pipe material may require different equivalent length factors. Verify other equivalent length factors. Verify other equivalent length factors with pipe material manufacturer. NOTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t = ft	Swing Check Valve		Х		=		1			7	
Globe Valve Globe Valve Butterfly Valve X - NOTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. Sum of Equivalent Length due to pipe fittings: Total Pipe Length - Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If the fit of the fittings and supply pipe (h _t): (10.5 \div Pipe Diameter ^{4.87}) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter ^{4.87}) X (Flow Rate \div Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 \div Pipe Diameter Diameter Constant) Difference (Line 3), the Distribution Head Loss (Line 4), Additional Head Loss (Line 4), Additional Head Loss (Line 4), Pipe Diameter Constant Const	Aprila Value		х		_		1				
Globe Valve Butterfly Valve X - NOTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. Sum of Equivalent Length due to pipe fittings: Total Pipe Length - Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t Hazen-Williams Equation for h $h_f = \frac{10.5}{D^{4.87}} * (Q \div C)^{1.85} * L$ Q in gpm L in feet D in inches C = 130 (10.5 ÷ Pipe Diameter ^{4.87}) X (Flow Rate * Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.5 † Pipe Diameter ^{4.87}) X (gpm + 130) ^{4.87} X Total Pipe Length (10.8) (10.5 † Pipe Length (10.8) (10.	Angle valve						ł			5.0	
Butterfly Valve $X = \frac{1}{1000} = \frac{10.5}{1000} = \frac{10.5}{10000} = \frac{10.5}{10000} = \frac{10.5}{100000} = \frac{10.5}{1000000000000000000000000000000000000$	Globe Valve		X		=						
Valve 10 Valve 10 Valve 11 X Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If the Hazen-Williams Faulation for h $h_f = \frac{10.5}{D^{4.87}} * (Q \div C)^{1.85} * L$ Q in gpm L in feet D in inches C = 130 (10.5 ÷ Pipe Diameter A-R7) X (Flow Rate + Constant) - R yellow Friction Loss (Line 8), nor Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. NOTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. NOTE: System installer should contact system designer if the number of fittings varies from the design to the actual installation. If the actual installation. Note: System installer should contact system the supply Pipe Length (10.A.) If the actual installation. NOTE: System installer should contact system the supply Fide Length (10.A.) If the actual installation. Note: System installer should contact system the supply Pipe Length (10.A.) If the actual installation. NOTE: System installer should contact system the supply Fide to the actual installation. Note: Plipe Length (10.8) If the actual installation. Note: System installer should contact system had begin to the actual installation. Note: $\frac{10.5}{D^{4.87}} * (Q \div C)^{1.85} * L$ In feet D in inches C = 130 In feet D in inches C			v				1		with pipe i	naccriac	
Valve 10 Valve 11 X Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t Hazen-Williams Fauation for h $h_f = \frac{10.5}{D^{4.87}} * (Q \div C)^{1.85} * L$ Hazen-Williams friction loss due to pipe fittings and supply pipe (h_f) : Q in gpm L in feet D in inches C = 130 (10.5 * Pipe Diameter ^{4.87}) X (Flow Rate * Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 * Pipe Diameter ^{4.87}) X (gpm + 130) ^{1.85} X Total Pipe Length (10.8) (10.5 * Qin gpm L in feet D in inches C = 130 (10.5 * Qin gpm L in feet	Butterfly Valve								hauld canta	st sustam	
Valve 11 Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.B) + Equivalent Pipe Length (9.A.) If t = If t Hazen-Williams Fauation for h $h_f = \frac{10.5}{D^{4.87}} * (Q \div C)^{1.85} * L$ Hazen-Williams friction loss due to pipe fittings and supply pipe (h_f): Q in gpm L in feet D in inches C - 130 (10.5 ÷ Pipe Diameter ^{4.87}) × (Flow Rate ÷ Constant) ^{1.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{1.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{1.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{1.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{1.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{4.85} × Total Pipe Length (10.B) (10.5 ÷ In ^{4.87}) × (In gpm + 130) ^{4.85} × Total Pipe Length (10.B) (10.5 ÷ In feet D in inches C - 130 (10.5 † In feet	Valve 10		Х		=		ł	50 ST 10 ST 10 ST			he
Sum of Equivalent Length due to pipe fittings: Total Pipe Length = Supply Pipe Length (5.8) + Equivalent Pipe Length (9.A.) If t =	Valve 11		Х		=					ries iroin (
(10.5 ÷ Pipe Diameter ^{4.87}) X (Flow Rate ÷ Constant) ^{1.85} X Total Pipe Length (10.8) (10.5 ÷ In ^{4.87}) X (gpm + 130) ^{1.85} X ft = ft Total Head requirement is the sum of the Elevation Difference (Line 3), the Distribution Head Loss (Line 4), Additional Head Loss (Line 2) and either Supply Friction Loss (Line 9), or Friction Loss from the Supply Pipe and Pipe Fittings for collection systems (Line 10.C) NOTE: Supply Friction Loss (Line 8) need ONLY be used if NOT a collection system. NOTE: Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. If t + 5 ft + 5 ft + 6 ft = 8.55 ft PUMP SELECTION Thereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws.					20000	:	Q				
Total Head requirement is the sum of the Elevation Difference (Line 3), the Distribution Head Loss (Line 4), Additional Head Loss (Line 5) and either Supply Friction Loss (Line 9), or Friction Loss from the Supply Pipe and Pipe Fittings for collection systems (Line 10.C) NOTE: Supply Friction Loss (Line 8) need ONLY be used if NOT a collection system. NOTE: Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. If t + 5 ft + 5 ft + 6 ft = 8.5 ft PUMP SELECTION A pump must be selected to deliver at least							_				
NOTE: Supply Friction Loss (Line 8) need ONLY be used if NOT a collection system. NOTE: Friction Loss (Line 8) need ONLY be used if NOT a collection system. NOTE: Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. If t + 5 ft + 5 ft + 6 ft = 28.5 ft PUMP SELECTION A pump must be selected to deliver at least	(10.5 ÷	in ^{4.87})	Х (gpm -	- 130) ^{1.85} X		ft =		ft	
NOTE: Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. The system is a	Total Head requirement and either Supply Fric	ent is the sum of tion Loss (Line 9	the <i>Ele</i>), or Fi	evation Difference riction Loss from	e (Lin the Si	e 3), the Distri	but Pip	tion Head Loss (Line 4), be Fittings for collection	, Additional n systems (L	Head Loss ine 10.C)	(Line 5),
NOTE: Friction Loss from the Supply Pipe and Pipe Fittings (Line 9.C) need ONLY be used if system is a collection system. The system is a	NOTE: Supply Frictio	n Loss (Line 8) r	eed O	NLY be used if N	ОТа	collection syst	ten	n.			
PUMP SELECTION A pump must be selected to deliver at least 18 GPM (Line 1 or Line 2) with at least 28 feet of total head. I hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws. Since Westerland Westerland 43 10/4/21											
a pump must be selected to deliver at least 18 GPM (Line 1 or Line 2) with at least 28 feet of total head. I hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws. Oveg Westerland 2004/21	2) ft + 5 ft + 2,15 ft + ft = 28,15 ft										
I hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws. Oveg Westerland Sugar Stephan 63 10/4/21	PUMP SELECTION										
Greg Westerland Sheawoterland 663 10/4/21	A pump must be selecte	ed to deliver at le	east	18 GPM	(Line	1 or Line 2) wi	th	at least 28	feet of to	tal head.	
oreg Westerland Leawesterland 663 10/4/21	I hereby certify that I had	ave completed thi	is work	in accordance wi	th all a	applicable ordin	an	ces, rules and laws.			
(Designer) (Signature) (License #) (Date)											

13-34 SECTION 13: Forms and Reference

(Designer)

OSTP Pump Tank Sizing, Dosing and Float and Timer Setting Design Worksheet Minnesota Pollution OF MINNESOTA Control Agency B. DEMAND DOSE FLOAT SETTINGS 18. Calculate Float Separation Distance using Dosing Volume. Total Dosing Volume (Line 12)/Gallons Per Inch (Line 2) gal ÷ 19. Measuring from bottom of tank: A. Distance to set Pump Off Float = Pump Height + Block Height (Line 5) + Alarm Depth (Line 13) B. Distance to set Pump On Float=Distance to Set Pump-Off Float (Line 19.A) + Float Separation Distance (Line 18) C. Distance to set Alarm Float = Distance to set Pump-On Float (19.B) + Alarm Depth (2-3 inches) in = 23 Inches FLOAT SETTINGS **DEMAND DOSING** TIMED DOSING Alarm Depth Pump Off in I hereby certify that I have completed this work in accordance with all applicable ordinances, rules and laws.

(Signature)

(License #)

13-32 SECTION 13: Forms and Reference

OSTP Pump Tank Sizing, Dosing and Float

Minnesota Pollution Control Agency

and Timer Setting Design Worksheet



DEI	ERMIN	E AREA AND/OR GALLON	S PER INCH			
1.	Α.	Rectangle area = Length	(L) X Width (W)	Width		
		11.5 ft	X = 508 ft =	58.42 ft2		
	В.	Circle area = $3.14r^2$ (3.1	4 X radius X radius)	Length		
		3.14 X	2 ft =	ft ² Radius		
	C.	Get area from manufact	urer	ft ²		
	D.	Get gallons per inch from	n manfufacture	Gallons per inch		
2.	Calcul	ate Gallons Per Inch :		Total transmitter and transmit		
	There tank h	are 7.48 gallons per cubicolds. Then divide that nu	c foot. Therefore, multiply the area fumber by 12 to calculate the gallons pe	rom 1.A, 1.B, or 1.C by 7.48 to determine the gallons per foot the er inch.		
	(Area	X 7.48 gallons/ft ³)/(12 in	/ft) =			
ı	00	. (1)				
-	28	642 X 7.	$48 \text{ gal/ft}^3 \div 12 \text{ in/ft} =$	36.43 Gallons per inch		
TAN	K CAP	ACITY				
3.	Enter	the Pump Tank Capacity (minimum provided in the table below): 500 Gallons		
4.	4. Calculate Total Tank Volume					
	A. Depth from bottom of inlet pipe to tank bottom:					
	В.	Total Tank Volume = De	pth from bottom of inlet pipe (Line 4	.A) X Gallons/Inch (Line 2)		
	in \times 36.42 Gallons Per Inch = 109266 Gallons					
5.	5. Calculate Volume to Cover Pump (The inlet of the pump must be at least 4-inches from the bottom of the					
	pump tank & 2 inches of water covering the pump is recommended)					
	(Pump and block height + 2 inches) X Gallons Per Inch (1D or 2)					
2	(1 disp and block height + 2 inches) X dations Per Inch (1) or 2) (1) or 2) (2) Gallons Per Inch (3) Gallons Per Inch (4) Gallons					
		Design Flow				
		(Gallons Per Minimum Pump Tank Capacity (Gallons)				
		Day)				
		0-600	500	or Altnernating Dual Pumps		
		601-4,999	100% of the Design Flow			
		5,000-9,999	50% of the Design Flow	and Altnernating Dual Pumps		

OSTP Pump Tank Sizing, Dosing and Float

UNIVERSITY and Timer Setting Design Worksheet Minnesota Pollution OF MINNESOTA Control Agency DOSING VOLUME 7. Minimum Pumpout Volume - 5 X Volume of Distribution Piping: Gallons - Line 17 of the Pressure Distribution or Line 11 of Non-level 8. Calculate Maximum Pumpout Volume (25% of Design Flow) Design Flow: GPD 0.25 Gallons 9. Select a pumpout volume that meets both items above (Line 7 & 8): Gallons 10. Calculate Doses Per Day = Design Flow : Dosing Volume Volume of Liquid in) gpd ÷ gal **Pipe** 11. Calculate Drainback: Pipe Liquid Diameter of Supply Pipe = inches Diameter Per Foot (inches) (Gallons) B. Length of Supply Pipe = 0.045 1 c. Volume of Liquid Per Lineal Foot of Pipe = Gallons/ft 1.25 0.078 D. Drainback = Length of Supply Pipe X Volume of Liquid Per Lineal Foot of Pipe 1.5 0.110 0.170 gal/ft 3 0.380 12. Total Dosing Volume = Dosing Volume (Line 9) plus Drainback (Line 11.D) 4 0.661 gal = 105 13. Minimum Alarm Volume = Depth of alarm (2 or 3 inches) X gallons per inch of tank (Line 1 or 2) 3(0+4/2) gal/in TIMER or DEMAND FLOAT SETTINGS Select Timer or Demand Dosing: Demand Dose A. Timer Settings 14. Required Flow Rate: A. From Design (Line 11 of Pressure Distribution or Line 10 of Non-Level*): GPM *Note: This value must be adjusted after field B. Or calculated: GPM = Change in Depth (in) x Gallons Per Inch (Line 1 or 2) / Time Interval in Minutes measurement & in X min = calculation. 15. Choose a Flow Rate from Line 14.A or 14.B above. GPM 16. Calculate TIMER ON setting: Total Dosing Volume (Line 12)/GPM(Line 15) gal ÷ Minutes ON 17. Calculate TIMER OFF setting: Minutes Per Day (1440)/Doses Per Day (Line 10) - Minutes On (Line 16) 1440 min doses/day min Minutes OFF 17. Pump Off Float - Measuring from bottom of tank: Distance to set Pump Off Float=Gallons to Cover Pump (Line 5) / Gallons Per Inch (Line 1 or 2): gal ÷ gal/in = Inches 18. Alarm Float - Measuring from bottom of tank: Distance to set Alarm Float = Tank Depth(4A) - Alarm Depth (Line 13) in =

CLIENT: Bruce Maples 16-0-03	DATE: 10/4/21
MAP DRAWN TO SCALE	11/4/
MAP DRAWN TO SCALE Nov	WITH A NORTH ARROW The Properties Well Brix Toe Toe Toe Toe Toe Toe Toe To
Zow Are	South prop. Time - 250 58 stock Rock bed
ACCESS ROUTE FOR TANK MAINTENANCE QUIRED SETBACKS STRUCTURES OHWL DMMENTS: ESIGNER SIGNATURE CENSE# COS ACCESS ROUTE FOR TANK MAINTENANCE PROPERTY LINES DESIGNER SIGNATURE DES	ING BEEN DRAWN ON THE MAP?? INDICATE ELEVATIONS BENCHMARK 100 - \$1000

University of Minnesota



Septic System Management Plan for Above Grade Systems

The goal of a septic system is to protect human health and the environment by properly treating wastewater before returning it to the environment. Your septic system is designed to kill harmful organisms and remove pollutants before the water is recycled back into our lakes, streams and groundwater.

This management plan will identify the operation and maintenance activities necessary to ensure long-term performance of your septic system. Some of these activities must be performed by you, the homeowner. Other tasks must be performed by a licensed septic maintainer or service provider. However, it is YOUR responsibility to make sure all tasks get accomplished in a timely manner.

The University of Minnesota's Septic System Owner's Guide contains additional tips and recommendations designed to extend the effective life of your system and save you money over time.

Proper septic system design, installation, operation and maintenance means safe and clean water!

Permit #	Date Inspected
Permitting Authority	Phone
Service Provider/Maintainer	Phone
System Installer Westerland Const.	License # 663
System Designer Greg Westerlund	License # 663
Property Address 19825 327Ave, Isle	Property ID /6-0-03530
Property Owner Bruce & Linda Mas	oles

Keep this Management Plan with your Septic System Owner's Guide. The Septic System Owner's Guide includes a folder designed to hold maintenance records including pumping, inspection and evaluation reports. Ask your septic professional to also:

- · Attach permit information, designer drawings and as-builts of your system, if they are available.
- Keep copies of all pumping records and other maintenance and repair invoices with this document.
- Review this document with your maintenance professional at each visit; discuss any changes in product use, activities or water-use appliances.

For a copy of the Septic System Owner's Guide, call 1-800-876-8636 or go to http://shop.extension.umn.edu/

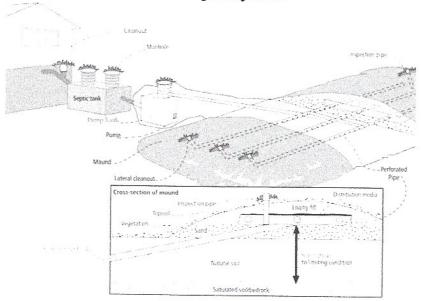
http://septic.umn.edu

13-86 SECTION 13: Forms and Reference

University of Minnesota

Septic System Management Plan for Above Grade Systems

Your Septic Systems Your Septic System



Septic System Specifics		
System Type: I II III IV* V* (Based on MN Rules Chapter 7080.2200 – 2400)	□ System is subject to operating permit* □ System uses UV disinfection unit* Type of advanced treatment unit *Additional Management Plan required	

Dwelling Type	Well Construction		
Number of bedrooms:	Well depth (ft):		
System capacity/ design flow (gpd):	Cased well Casing depth:		
Anticipated average daily flow (gpd):	Other (specify):		
Comments	Distance from septic (ft): 80 '+		
In-home business? What type?	Is the well on the design drawing?		

Septic Tank					
	One tank Tank volume: 600 gallons		Pump Tank (if one) 1,000 gallons		
			Effluent Pump type: Zoelle V		
	Two tanks Tank volume: gallons		TDH 18 Feet of head		
	Tank is constructed of Pre (957		Pump capacity 38 GPM		
	Effluent Screen type:		Alarm 1 visual audible		

Soil Treatmen	t Area
Mound/At-Grade area (length x width): 40 ft x 57 ft Rock bed size (length x width): 40 ft x 25 ft	☐ Cleanouts or Inspection Ports☐ Surface Water Diversions

SECTION 13: Forms and Reference ■ 13-87

University of Minnesota

Septic System Management Plan for Above Grade Systems



Homeowner Management Tasks

These operation and maintenance activities are your responsibility. Use the chart on page 6 to track your activities.

Identify the service intervals recommended by your system designer and your local government. The tank assessment for your system will be the shortest interval of these three intervals. Your pumper/maintainer will determine if your tank needs to be pumped.

System Designer:	check every 36	months		
oystem Designer.	check every	_ monus	My tonk near	ds to be checked
Local Government:	check every	months	IVIY talik lice	as to be checked
			everv	months
State Requirement:	check every 36	_months	_ cvciy _	months

Seasonally or several times per year

- Leaks. Check (listen, look) for leaks in toilets and dripping faucets. Repair leaks promptly.
- Surfacing sewage. Regularly check for wet or spongy soil around your soil treatment area. If surfaced sewage or strong odors are not corrected by pumping the tank or fixing broken caps, call your service professional. Untreated sewage may make humans and animals sick.
- Alarms. Alarms signal when there is a problem; contact your maintainer any time the alarm signals.
- Lint filter. If you have a lint filter, check for lint buildup and clean when necessary. Consider adding one after washing machine.
- Effluent screen. If you do not have one, consider having one added the next time the tank is cleaned.

Annually

- □ Water usage rate. A water meter can be used to monitor your average daily water use. Compare your water usage rate to the design flow of your system (listed on the next page). Contact your septic professional if your average daily flow over the course of a month exceeds 70% of the design flow for your system.
- Caps. Make sure that all caps and lids are intact and in place. Inspect for damaged caps at least every fall. Fix or replace damaged caps before winter to help prevent freezing issues.
- □ Water conditioning devices. See Page 5 for a list of devices. When possible, program the recharge frequency based on water demand (gallons) rather than time (days). Recharging too frequently may negatively impact your septic system.
- Review your water usage rate. Review the Water Use Appliance chart on Page 5. Discuss any major changes with your pumper/maintainer.

During each visit by a pumper/maintainer

- Ask if your pumper/maintainer is licensed in Minnesota.
- Make sure that your pumper/maintainer services the tank through the manhole. (NOT though a 4" or 6" diameter inspection port.)
- Ask your pumper/maintainer to accomplish the tasks listed on the Professional Tasks on Page 4.

13-88 SECTION 13: Forms and Reference

University of Minnesota

Septic System Management Plan for Above Grade Systems



Professional Management Tasks

These are the operation and maintenance activities that a pumper/maintainer performs to help ensure long-term performance of your system. Professionals should refer to the O/M Manual for detailed checklists for tanks, pumps, alarms and other components. Call 800-322-8642 for more details.

Written record provided to homeowner after each visit.

Plumbing/Source of Wastewater

- Review the Water Use Appliance Chart on Page 5 with homeowner. Discuss any changes in water use and the impact those changes may have on the septic system.
- Review water usage rates (if available) with homeowner.

Septic Tank/Pump Tanks

- ☐ Manhole lid. A riser is recommended if the lid is not accessible from the ground surface. Insulate the riser cover for frost protection.
- Liquid level. Check to make sure the tank is not leaking. The liquid level should be level with the bottom of the outlet pipe. (If the water level is below the bottom of the outlet pipe, the tank may not be watertight. If the water level is higher than the bottom of the outlet pipe of the tank, the effluent screen may need cleaning, or there may be ponding in the drainfield.)
- Inspection pipes. Replace damaged caps.
- Baffles. Check to make sure they are in place and attached, and that inlet/outlet baffles are clear of buildup or obstructions.
- Effluent screen. Check to make sure it is in place; clean per manufacturer recommendation.
 Recommend retrofitted installation if one is not present.
- Alarm. Verify that the alarm works.
- Scum and sludge. Measure scum and sludge in each compartment of each septic and pump tank, pump if needed.

Pump

- Pump and controls. Check to make sure the pump and controls are operating correctly.
- Pump vault. Check to make sure it is in place; clean per manufacturer recommendations.
- Alarm. Verify that the alarm works.
- Drainback. Check to make sure it is operating properly.
- □ Event counter or run time. Check to see if there is an event counter or run time log for the pump. If there is one, calculate the water usage rate and compare to the anticipated average daily flow listed on Page 2.

Soil Treatment Area

- Inspection pipes. Check to make sure they are properly capped. Replace caps that are damaged.
- Surfacing of effluent. Check for surfaced effluent or other signs of problems.
- Lateral flushing. Check lateral distribution; if cleanouts exist, flush and clean as needed.
- Ponding. Check for ponding. Excessive ponding in at-grade and mound beds indicates problems.

All other components - inspect as listed here:

University of Minnesota

Septic System Management Plan for Above Grade Systems



Water-Use Appliances and Equipment in the Home

Appliance	Impacts on System	Management Tips
Garbage disposal	 Uses additional water. Adds solids to the tank. Finely-ground solids may not settle. Unsettled solids can exit the tank and enter the soil treatment area. 	 Use of a garbage disposal is not recommended. Minimize garbage disposal use. Compost instead. To prevent solids from exiting the tank, have you tank pumped more frequently. Add an effluent screen to your tank.
Washing machine	 Washing several loads on one day uses a lot of water and may overload your system. Overloading your system may prevent solids from settling out in the tank. Unsettled solids can exit the tank and enter the soil treatment area. 	Choose a front-loader or water-saving top-loader
2 nd floor laundry	The rapid speed of water entering the tank may reduce performance.	 Install an effluent screen in the septic tank to prevent the release of excessive solids to the soil treatment area. Be sure that you have adequate tank capacity.
Dishwasher	 Powdered and/or high-phosphorus detergents can negatively impact the performance of your tank and soil treatment area. New models promote "no scraping". They have a garbage disposal inside. 	Use gel detergents. Powdered detergents may add solids to the tank. Use detergents that are low or no-phosphorus. Wash only full loads. Scrape your dishes anyways to keep undigested solids out of your septic system.
Grinder pump (in home)	Finely-ground solids may not settle. Unsettled solids can exit the tank and enter the soil treatment area.	Expand septic tank capacity by a factor of 1.5. Include pump monitoring in your maintenance schedule to ensure that it is working properly. Add an effluent screen.
Large bathtub (whirlpool)	Large volume of water may overload your system. Heavy use of bath oils and soaps can impact biological activity in your tank and soil treatment area.	 Avoid using other water-use appliances at the same time. For example, don't wash clothes and take a bath at the same time. Use oils, soaps, and cleaners in the bath or shower sparingly.
Clean Water Uses	Impacts on System	Management Tips
High-efficiency furnace	 Drip may result in frozen pipes during cold weather. 	Re-route water into a sump pump or directly out of the house. Do not route furnace recharge to your septic system.
Water softener fron filter Reverse osmosis	 Salt in recharge water may affect system performance. Recharge water may hydraulically overload the system. 	 These sources produce water that is not sewage and should not go into your septic system. Reroute water from these sources to another outlet, such as a dry well, draintile or old drainfield.
Surface drainage Footing drains	Water from these sources will likely overload the system.	 When replacing consider using a demand-based recharge vs. a time-based recharge. Check valves to ensure proper operation; have unit serviced per manufacturer directions

13-90 ■ SECTION 13: Forms and Reference

University of Minnesota

Septic System Management Plan for Above Grade Systems



Maintenance Log

Track maintenance activities here for easy reference. See list of management tasks on pages 3 and 4.

Activity	Date accomplished					
Check frequently:						
Leaks: check for plumbing leaks						
Soil treatment area check for surfacing						
Lint filter: check, clean if needed						
Effluent screen: if owner-maintained						
Check annually:						
Water usage rate (monitor frequency)						
Caps: inspect, replace if needed						
Water use appliances – review use						
Other:						
Notes:						
Mitigation/corrective action plan:						
the sewage treatment system on this propert this Management Plan are not met. I will pr	is my responsibility to properly operate and maintain y, utilizing the Management Plan. If requirements in omptly notify the permitting authority and take ew system, I agree to adequately protect the reserve tem."					
Property Owner Signature:	Date					
Management Plan Prepared By: Greg U	kster and Certification # 824					
Permitting Authority:	•					

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