

Subsurface Sewage Treatment System Management Plan

Property Owner: CRAIG BUCK Phone: 651-206-3518 Date: 9-17-2019
Mailing Address: 5435 St. Hwy 70 City: Pine City MN Zip: 55063
Site Address: 22889 210th Ave. City: McGrath MN Zip: 56350

This management plan will identify the operation and maintenance activities necessary to ensure long-term performance of your septic system. Some of these activities must be performed by you, the homeowner. Other tasks must be performed by a licensed septic service provider.

System Designer: check every -0- months.
Local Government: check every -0- months.
State Requirement: check every 36 months.

(State requirements are based on MN Rules Chapter 7080.2450, Subp. 2 & 3)

My System needs to be checked
every 36 months.

Homeowner Management Tasks

- ✓ *Leaks*—Check (look, listen) for leaks in toilets and dripping faucets. Repair leaks promptly.
 - ✓ *Surfacing sewage*—Regularly check for wet or spongy soil around your soil treatment area.
 - ✓ *Effluent filter*—Inspect and clean twice a year or more.
 - ✓ *Alarms*—Alarm signals when there is a problem. Contact a service provider any time an alarm signals.
 - Event counter or water meter*—Record your water use.
- N/A* recommend meter readings be conducted (circle one: DAILY WEEKLY MONTHLY)

Professional Management Tasks

- Check to make sure tank is not leaking
- Check and clean the in-tank effluent filter
- Check the sludge/scum layer levels in all septic tanks
- Recommend if tank should be pumped
- Check inlet and outlet baffles
- Check the drainfield effluent levels in the rock layer
- Check the pump and alarm system functions
- Check wiring for corrosion and function
- Check dissolved oxygen and effluent temperature in tank
- Provide homeowner with list of results and any action to be taken
- Flush and clean laterals if cleanouts exist

"I understand it is my responsibility to properly operate and maintain the sewage treatment system on this property, utilizing the Management Plan. If requirements in the Management Plan are not met, I will promptly notify the permitting authority and take necessary corrective actions. If I have a new system, I agree to adequately protect the reserve area for future use as a soil treatment system."

Property Owner Signature: Craig B.

Date: 9-17-2019

Designer Signature: Brian English

Date: 9/17/2019

FIELD EVALUATION SHEET

PRELIMINARY EVALUATION DATE 9/14/19, FIELD EVALUATION DATE 9/14/19
PROPERTY OWNER: Craig Buck PHONE 651-306-3518
ADDRESS: 22679 210th Ave. CITY, STATE, ZIP: McGrath
LEGAL DESCRIPTION:
PIN# 37-0-048500 SEC 31 T 45 R 23 TWP NAME White Pine
FIRE# LAKE/RIVER LAKE CLASS OHWL FT.

DESCRIPTION OF SOIL TREATMENT AREAS

	AREA #1	AREA #2	REFERENCE BM ELEV.	FT.
DISTURBED AREAS	YES <u> </u> NO <u>X</u>	YES <u> </u> NO <u> </u>	REFERENCE BM DESCRIPTION	<u>Bottom of Sibley Street</u>
COMPACTED AREAS	YES <u> </u> NO <u>X</u>	YES <u> </u> NO <u> </u>		
FLOODING	YES <u> </u> NO <u>X</u>	YES <u> </u> NO <u> </u>		
RUN ON POTENTIAL	YES <u> </u> NO <u>X</u>	YES <u> </u> NO <u> </u>		
SLOPE %	<u>11%</u>	YES <u> </u> NO <u> </u>		
DIRECTION OF SLOPE	<u>No</u>	YES <u> </u> NO <u> </u>		
LANDSCAPE POSITION	<u>Flat Plains</u>	YES <u> </u> NO <u> </u>		
VEGETATION TYPES	<u>Grass Field</u>	YES <u> </u> NO <u> </u>		

DEPTH TO STANDING WATER OR MOTTLED SOIL: BORING# 1 18, 1A 2D, 2, 2A

BOTTOM ELEVATION-FIRST TRENCH OR BOTTOM OF ROCK BED: #1 418 FT., #2 FT.

SOIL SIZING FACTOR: SITE #1 1.27, SITE #2

CONSTRUCTION RELATED ISSUES: Nope

LIC# L2006

SITE EVALUATOR SIGNATURE: Dave English

SITE EVALUATOR NAME: Dave English

TELEPHONE# 592-3606

LUG REVIEW

DATE

Comments:

SOIL BORING LOGS ON REVERSE SIDE

MOUND DESIGN WORK SHEET (For Flows up to 1200 gpd)

A. Average Design FLOW

Estimated 300 gpd (see figure A-1).
or measured 1000 x 1.5 (safety factor) = 1500 gpd

B. SEPTIC TANK Capacity

1,000 gallons (see figure C-1)

A-1: Estimated Sewage Flows in Gallons per Day

number of bedrooms	Class I	Class II	Class III	Class IV
2	300	225	180	60% of the values in the Class I, II, or III columns.
3	450	300	218	
4	600	375	256	
5	750	450	294	
6	900	525	332	
7	1050	600	370	
8	1200	675	408	

C. SOILS (refer to site evaluation)

1. Depth to restricting layer = 1.5 feet
2. Depth of percolation tests = — feet
3. Texture 1/27
Percolation rate ... mpi
4. Soil loading rate — gpd/sqft (see figure D-33)
5. Percent land slope — %

C-1: Septic Tank Capacities (in gallons)

Number of Bedrooms	Minimum Liquid Capacity	Liquid capacity with garbage disposal	Liquid capacity with disposal pit inside
2 or less	750	1125	1500
3 or 4	1000	1500	2000
5 or 6	1500	2250	3000
7, 8 or 9	2000	3000	4000

D. ROCK LAYER DIMENSIONS

1. Multiply average design flow (A) by 0.83 to obtain required rock layer area.
300 gpd x 0.83 sqft/gpd = 250 sqft
2. Determine rock layer width = 0.83 sqft/gpd x linear Loading Rate (LLR)
0.83 sqft/gpd x 10 gpd/sqft = 10 ft.
3. Length of rock layer = area ÷ width =
250 sqft (D1) ÷ 10 ft (D2) = 25 ft

E. ROCK VOLUME

1. Multiply rock area (D1) by rock depth of 1 ft to get cubic feet of rock
250 sqft x 1 ft = 250 cuft
2. Divide cuft by 27 cuft/cuyd to get cubic yards
250 cuft ÷ 27 cuyd/cuft = 9.3 cuyd
3. Multiply cubic yards by 1.4 to get weight of rock in tons
9.3 cuyd x 1.4 ton/cuyd = 13 tons

Mound LLR

< 120 MPI	≤ 12
≥ 120 MPI	≤ 6

F. SEWAGE ABSORPTION WIDTH

Absorption width equals absorption ratio (See Figure D-33)
times rock layer width (D2)

$$10 \times 1.5 \text{ ft} = 15 \text{ ft}$$

D-33: Absorption Width Sizing Table

Percolation Rate in Minutes per Inch (MPI)	Soil Texture	Loading Rate Gallons per day per square foot	Absorption Ratio
Faster than 5	Coarse Sand Medium Sand Loamy Sand Fine Sand Sandy Loam Loam Silty Loam Silt	1.20	1.00
6 to 10	Sandy Clay Loam Silty Clay Loam Clay Loam Clay	0.20	1.00
11 to 15	Sandy Clay Silty Clay Clay	0.10	2.00
16 to 45	Silty Clay Sandy Clay Clay	0.30	2.00
46 to 60	Sandy Clay Loam Silty Clay Loam Clay Loam Clay	0.45	2.00
61 to 120	Silky Clay Sandy Clay Clay	0.24	3.00
Slowest than 120*			

*Standard pipes for these will result in lesser performance

PUMP SELECTION PROCEDURE

1. Determine pump capacity:

A. Gravity distribution

1. Minimum required discharge is 10 gpm
2. Maximum suggested discharge is 45 gpm. For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device.

B. Pressure distribution

See pressure distribution work sheet

From A or B Selected pump capacity: 22.2 gpm

2. Determine pump head requirements:

A. Elevation difference between pump and point of discharge?

6.9 feet

B. Special head requirement? (See Figure at right - Special Head Requirements)

5.0 feet

C. Calculate Friction loss

1. Select pipe diameter 2 in

2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1).

Read friction loss in feet per 100 feet from Figure E-9

Friction Loss = 1.11 ft/100ft of pipe

3. Determine total pipe length from pump discharge to soil treatment discharge point. Estimate by adding 25 percent to pipe length for fitting loss. Total pipe length times 1.25 = equivalent pipe length

30 feet \times 1.25 = 37.5 feet

4. Calculate total friction loss by multiplying friction loss (C2)

in ft/100 ft by the equivalent pipe length (C3) and divide by 100.
 $= \frac{37.5}{100} \text{ ft} \times \frac{1.11}{100} + 100 = \frac{30.11}{100} \text{ ft}$

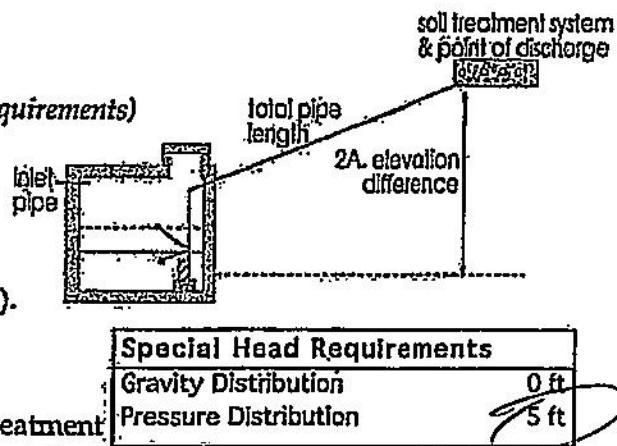
D. Total head required is the sum of elevation difference (A), special head requirements (B), and total friction loss (C4)

6.9 ft + 5 ft + 1.4 ft =

Total head: _____ feet

3. Pump selection

A pump must be selected to deliver at least 22.2 gpm
 (1A or B) with at least 12.3 feet of total head (2D)



flow rate gpm	E-9: Friction Loss in Plastic Pipe Per 100 feet		
	nominal pipe diameter 1.5"	2"	3"
20	2.47	0.73	0.11
25	3.73	1.11	0.16
30	5.23	1.55	0.23
35	6.96	2.06	0.30
40	8.91	2.64	0.39
45	11.07	3.28	0.48
50	13.46	3.99	0.58
55		4.76	0.70
60		5.60	0.82
65		6.48	0.95
70		7.44	1.09

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

Barb English

(signature)

10006

(license #)

9/17/2019

(date)

PRESSURE DISTRIBUTION SYSTEM

1. Select number of perforated laterals, 3

2. Select perforation spacing = 2.5 ft

3. Since perforations should not be placed closer than 1 foot to the edge of the rock layer (see diagram), subtract 2 feet from the rock layer length.

$$\begin{array}{c} \overline{25} \\ \text{Rock layer length} - 2 \text{ ft} = \overline{23} \text{ ft} \end{array}$$

4. Determine the number of spaces between perforations. Divide the length (3) by perforation spacing (2) and round down to nearest whole number.

$$\text{Perforation spacing} = \overline{23} \text{ ft} + \overline{25} \text{ ft} = \underline{\underline{9}} \text{ spaces}$$

5. Number of perforations is equal to one plus the number of perforation spaces (4). Check figure E-4 to assure the number of perforations per lateral guarantees <10% discharge variation.

$$\underline{\underline{9}} \text{ spaces} + 1 = \underline{\underline{10}} \text{ perforations/lateral}$$

6. A. Total number of perforations = perforations per lateral (5) times number of laterals (1)

$$\underline{\underline{10}} \text{ perfs/lat} \times \underline{\underline{3}} \text{ lat} = \underline{\underline{30}} \text{ perforations}$$

B. Calculate the square footage per perforation.

Should be 6-10 sqft/perf. Does not apply to at-grade.
Rock bed area = rock width (ft) x rock length (ft)

$$\underline{\underline{10}} \text{ ft} \times \underline{\underline{25}} \text{ ft} = \underline{\underline{250}} \text{ sqft}$$

Square foot per perforation = Rock bed area ÷ number of perfs (6)

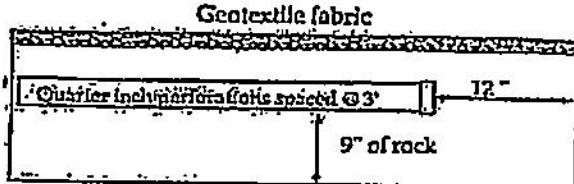
$$\underline{\underline{250}} \text{ sqft} \div \underline{\underline{30}} \text{ perfs} = \underline{\underline{8.3}} \text{ sqft/perf}$$

7. Determine required flow rate by multiplying the total number of perforations (6A) by flow per perforation (see figure E-6)

$$\underline{\underline{30}} \text{ perfs} \times \underline{\underline{74}} \text{ gpm/perf} = \underline{\underline{222}} \text{ gpm}$$

8. If laterals are connected to header pipe as shown on upper example, to select minimum required lateral diameter; enter figure E-4 with perforation spacing (2) and number of perforations per lateral (5). Select minimum diameter for perforated lateral = 1/2 inches.

9. If perforated lateral system is attached to manifold pipe near the center, lower diagram, perforated lateral length (3) and number of perforations per lateral (5) will be approximately one half of that in step 8. Using these values, select minimum diameter for perforated lateral = X inches.



E-4: Maximum allowable number of 1/4-inch perforations per lateral to guarantee <10% discharge variation.

perforation spacing (feet)	1 inch	1.25 inch	1.5 inch	20 inch
2.5	8	14	18	28
3.0	8	13	17	26
3.3	7	12	16	25
4.0	7	11	15	23
5.0	6	10	14	22

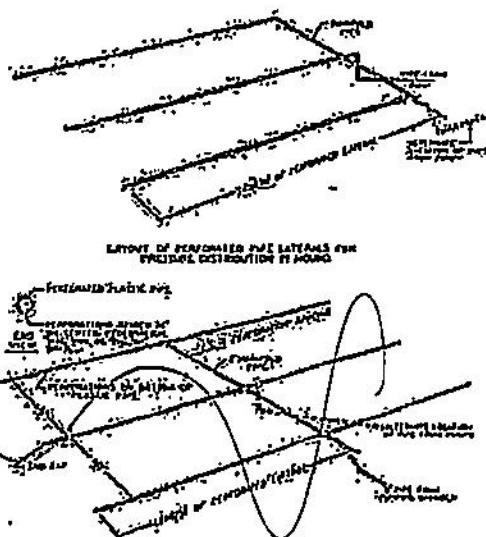
E-6: Perforation Discharge in gpm

head (feet)	perforation diameter (inches)			
	1/8	3/16	7/32	1/4
1.0 ^a	0.18	0.42	0.56	0.74
2.0 ^b	0.26	0.59	0.80	1.04
5.0	0.41	0.94	1.26	1.65

^a Use 1.0 foot for single-family homes.

^b Use 2.0 feet for anything else.

MANIFOLD LOCATED AT END OF PRESSURE DISTRIBUTION SYSTEM



I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.



(signature)

12-006

(license #)

8/17/2019

(date)

G. Mound Slope Width and Length
(landslope less than or equal to 1%)

$\leq 1\%$ land slope

1. Absorption width (F) 15 ft.

2. Calculate mound size

a. Determine depth of clean sand fill
at upslope edge of rock layer = 3 ft

minus the distance to restricting layer (C1)

$$3 \text{ ft} - 1.5 \text{ ft} = 1.5 \text{ ft}$$

b. Mound height at the upslope edge of rock layer = depth of clean sand for separation (G2a)

at upslope edge plus depth of rock layer (1 ft) plus depth of cover (1 ft)
1.5 ft + 1ft + 1ft = 3.5 ft

c. Berm width = upslope mound height (G2b) times 4 (4 is recommended, but could be 3-12)
3.5 x 4 = 14 ft

d. The total landscape width is the sum of berm (G2c) width plus rock layer width (D2) plus berm width (G2c): 14 ft + 10 ft + 14 ft = 38 ft

e. Additional width necessary for absorption = absorption width (F) minus the landscape width (G2d)

$$15 \text{ ft} - 38 \text{ ft} = \underline{\quad} \text{ ft}, \text{ if number is negative } (<0) \text{ skip to g}$$

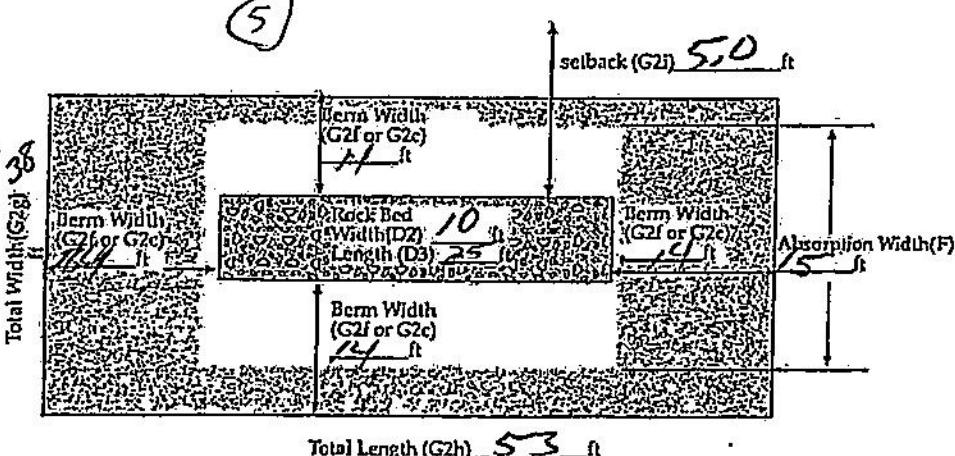
f. Final berm width = additional width (G2e) plus the berm width (G2c)

$$\underline{\quad} \text{ ft} + \underline{\quad} \text{ ft} = \underline{\quad} \text{ ft}$$

g. Total mound width is the sum of berm width (G2f or G2c) plus rock layer width (D2) plus berm width (G2f or G2c): 14 ft + 10 ft + 14 ft = 38 ft

h. Total mound length is the sum of berm (G2f or G2c) plus rock layer length (D3) plus berm (G2f or G2c): 14 ft + 25 ft + 14 ft = 53 ft

i. Setbacks from the rockbed are calculated as follows: the absorption width (F) minus the rock bed width (D2) divided by 2: (15 ft - 10 ft) \div 2 = 2.5 ft



Final Dimensions:

38 x 53

I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

(signature)

62006 (license #)

7/14/2018 (date)

MOUND CROSS-SECTION

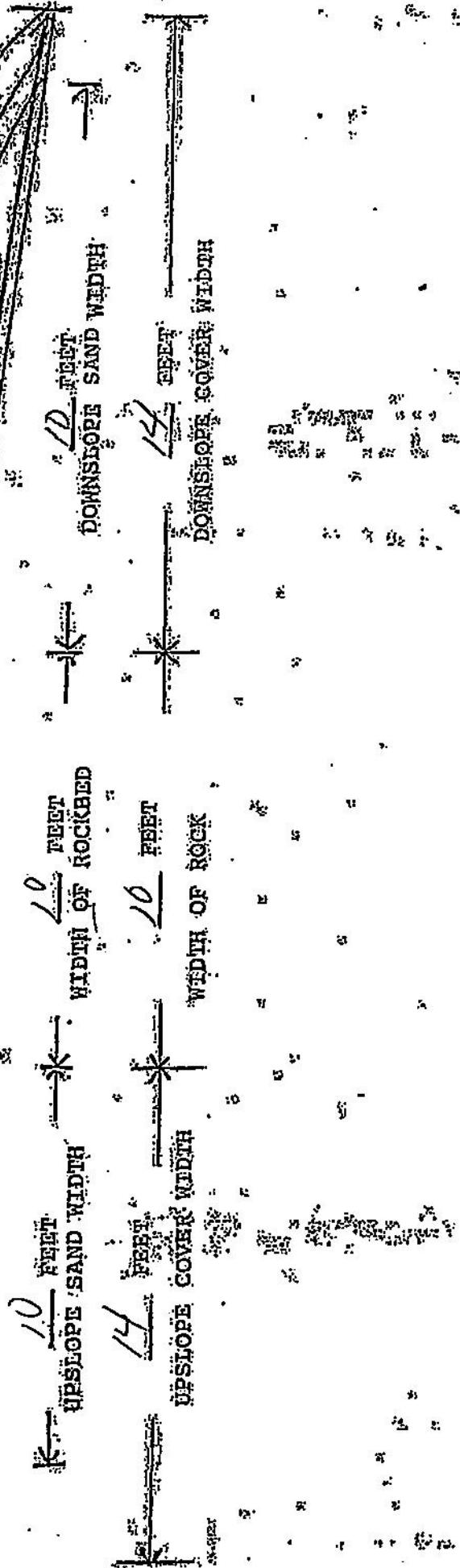
PERCENT SLOPE OF
ORIGINAL SOIL

10 FT. X 36 FT. SIZE OF ROCKBED 24 FT. X 45 FT. SIZE OF SANDBASE

GEOTEXTILE CLOTH

4 INCHES OF TOPSOIL FOR
GRASS COVER.
14 INCHES OF SANDY LOAM SOIL
TAPERING TO 8 INCHES
9" ROCK BELOW DISTRIBUTION PIPE
12 INCHES OF SAND
ROUGHENED SOIL SURFACE

ORIGINAL SECTION



CRATE BUCK

