# **Ekelund Excavating Inc**

50414 lily Ave McGregor MN 55760 218-426-4285

Lic#L552

George Haapoja

45621 St Hwy 65 McGregor MN 55760

Parcel# 14-0-000402

Sewer Design

MOUND DESIGN WORK SHEET (For Flows up	o to 120	00 gpd)				
A. Average Design FLOW	A-1: Es	timated Se	wage Flot	vs in G	allons per D	ay
Estimated <u>USO</u> gpd (see figure A-1) or measured x 1.5 (safety factor) = gpc  B. SEPTIC TANK Capacity	numbe bedroo 2 3 4 5	ms C	lass I 300 150 500 750	Class II 225 300 375 450	Class III 180 218 256 294	Class IV 60% of the values in the
	6 7 8	10	200 250 200	525 600 675	332 370 408	Class I, II, or III columns.
C SOTT S (refer to site multiplian)		C-1: Septic	Tank Capaciti	es (in galle	ons)	
C. SOILS (refer to site evaluation)  1. Depth to restricting layer = < 1 feet		Number of Bedrooms	Minimum Li Capacity	quid Lie	quid capacity with	Liquid capacity with disposal& lift inside
<ol> <li>Depth to restricting layer = feet</li> <li>Depth of percolation tests = feet</li> <li>Texture mpi</li> </ol>		2 or less 3 or 4 5 or 6 7, 8 or 9	750 1000 1500 2000		1125 1500 2250 3000	1500 2000 3000 4000
4. Soil loading rategpd/sqft (see figure 5. Percent land slope%	: D-33)					
D. ROCK LAYER DIMENSIONS				Antonyo Company		
<ol> <li>Multiply average design flow (A) by 0.83 to obtain</li></ol>			(LLR)	un	d LLR MPI	<u>.</u> ≤12
E. ROCK-VOLUME			≥ ]	20 1	MPI	≤6
<ol> <li>Multiply rock area (D1) by rock depth of 1 ft to get 360 sqft x 1 ft = 380 cuft</li> <li>Divide cuft by 27 cuft/cuyd to get cubic yards 240 cuft ÷ 27 cuyd/cuft = 14 cuyd</li> <li>Multiply cubic yards by 1.4 to get weight of rock in cuyd x 1.4 ton/cuyd = 1916 tons</li> </ol>	M (Sc.	eet of ro	ck	224		
*		D-33: Absor	ption Width	Sizing T	able	
F. SEWAGE ABSORPTION WIDTH		Percolation F in Minutes J Inch (MPI)		lure	Gallons per day per square feet	Absorption Ratio
Absorption width equals absorption ratio (See Figure D-	33)	Faster than	S Coarse S Medium Loamy S Fine Sa	Sand Sand ind	0.79	1.00
times rock layer width (D2)	Account of the second	16 to 30 31 to 45	Lorn Silt Lo Silt	am	0.60	2.00
$10 \times 267 \text{ ft} = 27 \text{ ft}$		46 to 60	Simly Clay Silly Clay Clay Lo	Loan Loan	0.45	2.67
		6) 10 120	Silty C	lay	0.24	5.00

Slower than 120°

\*System designed for these sails must be other or perfor

G. Mound Slope Width and Length	(41)
(landslope less than or equal to 1%)	alope ratio
1. Absorption width (F) 17 ft	6 Topsoit
2. Calculate mound size	
a. Determine depth of clean sand fill	Restricting Layer School
at upslope edge of rock layer = 3 ft 5 and Berm Whith (GZI or GZc)	Rock Width(D2) Berm Width (G2f or C2c)
minus the distance to restricting layer (C1)	Sand Absorption Width (F)
3 ft - 6 ft = 3 ft  b. Mound height at the upslope edge of rock layer = depth of clean sand for separation (G2a) at upslope edge plus depth of rock layer (1 ft) plus depth of cover  3 ft + 1ft + 1ft = 6 ft  c. Berm width = upslope mound height (G2b) times 4 (4 is recomm  \$\sum_{\s\	
d. The total landscape width is the sum of berm (G2c) width plus (G2c): $\frac{20}{10}$ ft + $\frac{10}{10}$ ft + $\frac{10}{10}$ ft = $\frac{50}{10}$ ft	rock layer width (D2) plus berm widt
e. Additional width necessary for absorption = absorption width	F) minus the landscape width (C2d)
97  ft - 50  ft = -23  ft, if number is negative (<0) ski	o to g
f. Final berm width = additional width (G2e) plus the berm width	
$\underline{\qquad \qquad ft + \underline{\qquad ft = \qquad ft}}$	į v
g. Total mound width is the sum of berm width (G2f or G2c) plus width (G2f or G2c): $2 \circ \text{ft} + 10 \circ \text{ft} + 20 \circ \text{ft} = 50 \circ \text{ft}$	rock layer width (D2) plus berm
h. Total mound length is the sum of berm (G2f or G2c) plus rock length: $\frac{1}{2}$ ft + $\frac{1}{2}$ ft = $\frac{1}{2}$ ft	ayer length (D3) plus berm (G2f or
i. Setbacks from the rockbed are calculated as follows: the absorption (D2) divided by 2: $(27 \text{ ft} - 60 \text{ ft}) \div 2 = 6.6 \text{ ft}$	on width (F) minus the rock bed widtl
	setback (G2i) 8-5 ft
Final Dimensions:  So X 76  Berm Width (C2f or C2c)  Berm Width (C2f or G2c)  1  Berm Width (C2f or G2c)  1  Berm Width (C2f or G2c)  20 It  Berm Width (C2f or G2c)  1  Berm Width (C2f or G2c)  1  Berm Width (C2f or G2c)  1  Berm Width (C2f or G2c)	Berm Width  Absorption Width  (G2f or G2c)  Absorption Width(F)
Berm Width (G2f or G2c)  10 1  Total Length (G2h)	78 s
I hereby certify that I have completed this work in accordance with applicable or (signature)	dinances, rules and laws. #) 5/90/16(date)

DDTCCTIDT	DISTRIBUTION	CALCULATE
		A 20 1 12 10 11

- Select perforation spacing = 3 ft
- Since perforations should not be placed closer than 1 foot to the edge of the rock layer (see diagram), subtract 2 feet from the rock layer length.

Determine the number of spaces between perforations. Divide the length (3) by perforation spacing (2) and round down to nearest whole number.

Perforation spacing = 36 ft ÷ 3 ft = 12 spaces

Number of perforations is equal to one plus the number of perforation spaces(4). Check figure E-4 to assure the number of perforations per lateral guarantees <10% discharge variation.

 $_{\text{spaces}} + 1 = \frac{13}{12}$  perforations/lateral

A. Total number of perforations = perforations per lateral (5) times number of laterals (1)

13 perfs/lat x 3 lat = 39 perforations

B. Calculate the square footage per perforation. Should be 6-10 sqft/perf. Does not apply to at-grades. Rock bed area = rock width (ft) x rock length (ft)

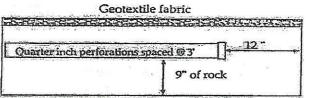
in ftx 3% ft = 3% sqft Square foot per perforation = Rock bed area ÷ number of perfs (6)

360 sqft ÷ 35 perfs = 9.7 sqft/perf

7. Determine required flow rate by multiplying the total number of perforations (6A) by flow per perforation (see figure E-6)

39 perfs x 80 gpm/perfs = 31.2 gpm

- 8. If laterals are connected to header pipe as shown on upper example, to select minimum required lateral diameter; enter figure E-4 with perforation spacing (2) and number of perforations per lateral (5) Select minimum diameter for perforated lateral = 1/4 inches.
- If perforated lateral system is attached to manifold pipe near the center, lower diagram, perforated lateral length (3) and number of perforations per lateral (5) will be approximately one half of that in step 8. Using these values, select minimum diameter for perforated lateral = 1" inches.



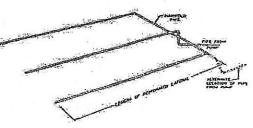
Perf Sizing 3/16" - 1/4" Perf Spacing 1.5'- 5'

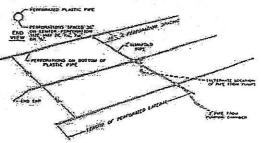
E-4: Maximum allowable number of 1/4-inch perforations per lateral to guarantee <10% discharge variation

perforation spacing (leet)	1 inch	1.25 inch	1.5 inch	20 inch
2.5	8	14	18	28
(3.0)	8	- 13	(1)	26
3.3	7	12	16	25
4.0	7	11	15	23
5.0	6	10	14	22

• •		perforation diameter (inches)						
head (feet)	1/8	3/16	7/32	1/4				
1.00	0.18	0.42	0.56	0.74				
2.0b	0.26	0.59	0.80	1.04				
5.0	0.41	0.94	1.26	1.65				

MANIFOLD LOCATED AT END OF PRESSURE DISTRIBUTION SYSTEM





I hereby certify that I have completed this work in accordance with applicable ordinances, rules and laws.

(signature) <u>4559</u> (license #) <u>5/10/16</u>

\_(date)

### PUMP SELECTION PROCEDURE

### 1. Determine pump capacity:

### A. Gravity distribution

3. Pump selection

A pump must be selected to deliver at least 32 gpm (1A or B) with at least 17.5 feet of total head (2D)

- 1. Minimum required discharge is 10 gpm
- 2. Maximum suggested discharge is 45 gpm. For other establishments at least 10% greater than the water supply rate, but no faster than the rate at which effluent will flow out of the distribution device.
- B. Pressure distribution See pressure distribution work sheet

From A or B Selected pump capacity:gpm					
2. Determine pump head requirements:					
A. Elevation difference between pump and point of discharge?  great					ment system of discharge
B. Special head requirement? (See Figure at right - Special Head Requirement	ts)	total pipe	-		
			2A. elev		
C. Calculate Friction loss pipe			differe	ence	
1. Select pipe diameter 1-5 in		5 T. #8474.0			
2. Enter Figure E-9 with gpm (1A or B) and pipe diameter (C1).					/ 6
Read friction loss in feet per 100 feet from Figure E-9	Special H	ead Re	quire	ments	1
Friction Loss = 6.96 ft/100ft of pipe	Gravity Dis				0 ft
3. Determine total pipe length from pump discharge to soil treatment	Pressure Di	stributio	חמ		5 ft
discharge point. Estimate by adding 25 percent to pipe length for		1.		1 -4	
fitting loss. Total pipe length times 1.25 = equivalent pipe length $40$ feet $\times$ 1.25 = $50$ feet	E-9: Friction	on Loss i Per 100		c Pipe	e s
4. Calculate total friction loss by multiplying friction loss (C2)		7.5	ominal		
in ft/100 ft by the equivalent pipe length (C3) and divide by 100.  = $\frac{1.96}{6}$ ft/100ft × $\frac{50}{6}$ ÷100 = $\frac{3.48}{6}$ ft	flow rate gpm	1.5"	e diam 2"	3" eier	
D. Total head required is the sum of elevation difference (A), special	20	2.47	0.73	0.11	
head requirements (B), and total friction loss (C4)	25	3.73	1.11	0.16	
9 ft + 5 ft + 3.48 ft =	30	5.23	1.55	0.23	
Total head: 17-4 feet	35	6.96	2.06	0.30	

E-9. PROI			c Libe
flow rate		reer nomina e diam 2"	
20	2.47	0.73	0.11
25	3.73	1.11	0.16
30	5.23	1.55	0.23
35	6.96	2.06	0.30
40	8.91	2.64	0.39
45	11.07	3.28	0.48
50	13.46	3.99	0.58
55	-	4.76	0.70
60		5.60	0.82
65		6.48	0.95
70		7.44	1.09

ereby certify that I have complete	d this work in accor	dance with app	olicable ordinar	nces, rules and la	iws.
Inhoon	(signature)			5/20/10	(date)

## DOSING CHAMBER SIZING

	-	-
1. Determine area	i 11 ×	
	Width T :	
A. Rectangle area = L x W		
x =square feet		
B. Circle area = $\pi$ (3.14) x radius in feet x radius in feet	Length	
$3.14 \times _{ft \times _{ft}} $ ft =sqft		
C. Get area from manufacturersqft	Radius	Ì
		7
2. Calculate gallons per inch		<i>}</i>
	(1 A P (1)	
There are 7.5 gallons per cubic foot of volume, therefore multiply the area		
times the conversion factor and divide by 12 inches per foot to calculate ga		
Area x 7.5 ÷ 12 = $\frac{\text{sqft} \times 7.5 \div 12 \text{ in/ft}}{\text{gallon per inch}}$	1	
	Legal Tank	:
3. Calculate total tank volume	500 gallons of	
A. Depth from bottom of inlet pipe to tank bottomin	4000/ 47 TO 17	
B. Total tank volume = depth from bottom of inlet pipe to tank bottom (3A)	) x gal/in (2) 100% the Daily	flow
=	or	
· · · · · · · · · · · · · · · · · · ·	Alternating Pur	mms
4. Calculate gallons to cover pump (with 2-3 inches of water covering pump)		or , amount
(Pump and block height (inch) + 2 inch) x gallon/inch	A-1: Estimated Sewage Rows in Gallons per D	)my
( $\frac{3}{\sin + 2 \text{ in}} \times \frac{1264 \text{ gal/in}}{2 \text{ gal/in}} = \frac{19635 \text{ gallon}}{2 \text{ gallon}}$	number of	
The state of the s		Closs IV
5. Calculate total pumpout volume		60%
A. Select pump size for 4-5 does per day. Gallon per dose = gpd (see figure A.		of the
		1 1
/ doses per day = 450 gpd ÷ 4 doses/day = 1125 gallons		volues
B. Calculate drainback	5 750 450 294	inthe
1. Determine total pipe length, 40 feet	6 900 525 332	Closs I.
2. Determine liquid volume of pipe, gal per ft (see figure E-20)	7 1050 600 370	LorM
3. Drainback quantity = 40 ft (5B1) x 11 gal per ft (5B2) = 44	gal 8 1200 675 408	columns
C. Total pump out volume = dose volume (5A) + drainback (5B3)	***	—i
112.5 gal + $4.5$ gal = $117$ Total gallon	E-20: Volume of Liquid in Pip	e 1
	D D D	
6. Float separation distance (using total pumpout volume)	Pipe Diameter Gallons per	toot
Total pumpout volume (5C) ÷ gal/inch (2)	inches	
17 gal ÷ $126$ gal/in= $9.2$ inch	1 0.045	1
	1.25 0.078	1
7. Calculate volume for alarm (typically 2 to 3 inches)	1.5 0.11	
Alarm depth (inch) x gallon/inch (2) = $\frac{3}{3}$ in x $\frac{12.69}{9}$ gal/in) = $\frac{3}{3}$ gal	al 2 0.17	
Add in deput (inch) x gation/ inch (2) =/ in x _1z v gar/ in) =/ gar	25 0.25	1
0 601 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	War and The Control of the Control o	1
8. Calculate total gallon = gallons over pump (4) + gallons pumpout (5C) + gal	llons alarm (7) 3 0.38	1
110 gal + 117 gal + 39 gal = 374 gallons	4 0.66	
	Trains and	
9. Total Tank Depth,= total gallon (8) ÷ gallon/inch (2)	E Control of the Cont	
$\frac{274}{\text{gal}} \div \frac{12.69}{\text{gal/in}} = \frac{21.5}{\text{in}}$ in		
inle		
pipe	e 🖄 Ť	
Recommended:		alarm d
		1 11 11 11 11 11 1
Calgulate reports compaits (75%) the deily flow)	S. Castivo copcioni	
Calculate reserve capacity (75% the daily flow)	S. Castivo copcioni	
D-11- 0		
	volume	control np on
D-11- 0	volume pun	control np on
D-11- 0	volume pump off pump con	control np on
D-11- 0	volume pun	control np on
D-11- 0	volume pump off pump con	control np on
Daily flow x .75 = $\frac{450}{0}$ x .75 = $\frac{337}{0}$ gallons pumpout	volume pump off con	control np on
D-11- 0	volume pump off con	control np on
Daily flow $x.75 = 450 \times .75 = 337$ gallons pumpout value of the pumpout of the	pump off con conirol see ordinances, rules and laws.	control np on
Daily flow x .75 = $\frac{450}{0}$ x .75 = $\frac{337}{0}$ gallons pumpout	pump off con conirol see ordinances, rules and laws.	control np on
Daily flow $x.75 = 450 \times .75 = 337$ gallons pumpout value of the pumpout of the	pump off con conirol see ordinances, rules and laws.	control np on

# SOILS CHARTS FOR BOTH PROPOSED AND ALTERNATE SITES

### 1 (PROPOSED) SOILS DATA

# (INCHES) COLOR O-6 TOPSOIL 6-10" Sondy form 7:5-48 5/6 modding

# 2 (PROPOSED) SOILS DATA

DEPIR	IECTURE MUNSELE	~ 1.5~~ ·
(INCHES)	· · · · · · · · · · · · · · · · · · ·	
0-6"	TopSoil .	2 2.
6 - 12 -		
0-12	Sandy lown 75/R 5/6 Mc	- , 7
	5/6 MG	ettlef
±*		
	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
		٠,
•		
•		
	ite start in	
	# #	

### 1 (ALTERNATE) SOILS DATA

1146-23	S)-479	Sime of	-	.35: C	OLO	R		
				•				
Ø			•.					
							_	
	•							
-					-		-	
•						-		
•		. <b>.</b> . • '			9			-
							-	
		5 <del></del>	•					
	-							
•					200			
1.50							•-	•
							•	
			-					
	•							
		125		جر. •	40		•	

### 2 (ALTERNATE) SOILS DATA

IN	Ć.	ES).	3.0					<u></u>		7°'.	
	).( <b></b> )		n.	•				•	(10)		•
	100 100 100 100 100 100 100 100 100 100		į.	*	٠,				· .	:	
••			14	•	*		•	-	•	•	
			•	6	•	•	٠		i=:		; - `.
•11			٠					3 <b>-</b>	-	•-	
•		- <sub>2</sub> -				*	•	•	<b>E</b>	ē	
*	100			110-						•	

ADDITIONAL SOIL BORINGS MAY BE REQUIRED

3 Dedleon 3 Good best wand Dol Sewer line 531 1650 combo Do furfline 0 582 78450 1 60, Righotory + 10, Setmer Hwy 65

100

991

971

SOIL BORINGS

#2

NAME George harbly PARCEL# 14-0-000 402

DISTRIBUTION DEVICE 1035
DIFFERENCE BETWEEN PUMP & DISCHARGE

**ELEVATIONS:** 

BENCH MARK

TANK INLET

PUMP

SEWER LINE @ HOUSE

BOTTOM OF ROCK RESTRICTIVE LAYER

DISTRIBUTION DEVICE

TOTAL PIPE LENGTH

# Subsurface Sewage Treatment System Management Plan

Property Owner: 6 longe Haalda	Phone: 🧳	18-820-5412	Date: 5/20/16
Mailing Address:	City:		Zip:
Site Address: 45621 Salguy 65	City: <u>Mc(</u>	ingd.	Zip: <u>55160</u>
This management plan will identify the operation an performance of your septic system. Some of these as must be performed by a licensed septic service proving System Designer:  Check every	ctivities must be pe ider. months.	rformed by you, the	homeowner. Other tasks
(State requirements are based on MN Rules Chapter 7080.2450,	Subp. 2 & 3)		
Homeowner Management Tasks  Lewks — Check (look, listen) for leaks  Surfacing sewage — Regularly check to  Effluent filter — Inspect and clean twi  Alarms — Alarm signals when there is  Event counter or water meter — Reconnected meter — Reconnected meter readings	for wet or spongy so ice a year or more. s a problem. Contac ord your water use.	oil around your soil to	reatment area.
Professional Management Tasks	100 TO 10		1.24882.1
☐ Check to make sure tank is n	N-Book		
Check and clean the in-tank		* 50 800	
☐ Check the sludge/scum layer		anks	
Recommend if tank should b			
☐ Check inlet and outlet baffle			
☐ Check the drainfield effluent		iyer	
☐ Check the pump and alarm s			
☐ Check wiring for corrosion ar		Carl 1991 39	Frankling of the second
☐ Check dissolved oxygen and			
☐ Provide homeowner with list	1780	action to be taken	
☐ Flush and clean laterals if cle	anouts exist		
"I understand it is my responsibility to properly operate an Management Plan. If requirements in the Management Planecessary corrective actions. If I have a new system, I agre system."	an are not met, I will	promptly notify the per ect the reserve area for	rmitting authority and take r future use as a soil treatment
Property Owner Signature:	Tarpaja	Date	: 5-20-16
Designer Signature:		Date	: 5-20-16 : 5/90/16

See Reverse Side for Management Log